Supplementary Material

Polarizability tensor invariants of H₂, HD, and D₂

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List of symbols

- α_{\perp} : polarizability perpendicular to the internuclear axis
- α_{\parallel} : polarizability parallel to the internuclear axis
- $\bar{\alpha}^{"}$: mean polarizability, $\bar{\alpha} = (2\alpha_{\perp} + \alpha_{\parallel})/3$ $\gamma^{"}$: polarizability anisotropy, $\gamma = \alpha_{\parallel} \alpha_{\perp}$

S1. Matrix elements of mean polarizability

						,		,			
$\lambda(\text{nm})$	$\langle \bar{\alpha} \rangle_{00,00}$	$\langle \bar{\alpha} \rangle_{10,10}$	$\langle \bar{\alpha} \rangle_{10,00}$	$\langle \bar{\alpha} \rangle_{11,01}$	$\langle \bar{\alpha} \rangle_{12,02}$	$\langle \bar{\alpha} \rangle_{13,03}$	$\langle \bar{\alpha} \rangle_{14,04}$	$\langle \bar{\alpha} \rangle_{15,05}$	$\langle \bar{\alpha} \rangle_{16,06}$	$\langle \bar{\alpha} \rangle_{17,07}$	$\langle \bar{\alpha} \rangle_{18,08}$
182.26	7.1074	8.0375	1.2674	1.2706	1.2771	1.2867	1.2996	1.3158	1.3354	1.3583	1.3846
193.00	6.8667	7.7165	1.1819	1.1847	1.1903	1.1987	1.2099	1.2239	1.2408	1.2605	1.2832
213.00	6.5441	7.2947	1.0729	1.0752	1.0798	1.0866	1.0958	1.1073	1.1211	1.1371	1.1555
222.00	6.4350	7.1541	1.0374	1.0395	1.0438	1.0503	1.0588	1.0695	1.0823	1.0973	1.1143
224.30	6.4098	7.1218	1.0293	1.0314	1.0356	1.0420	1.0504	1.0609	1.0735	1.0882	1.1049
235.00	6.3047	6.9876	0.9960	0.9979	1.0019	1.0078	1.0157	1.0255	1.0372	1.0509	1.0664
248.00	6.1991	6.8536	0.9631	0.9649	0.9686	0.9741	0.9814	0.9906	1.0015	1.0142	1.0286
266.00	6.0824	6.7067	0.9276	0.9293	0.9327	0.9377	0.9445	0.9529	0.9630	0.9747	0.9879
275.36	6.0322	6.6438	0.9125	0.9141	0.9174	0.9223	0.9289	0.9370	0.9467	0.9579	0.9707
285.00	5.9864	6.5866	0.8989	0.9005	0.9036	0.9084	0.9147	0.9226	0.9320	0.9429	0.9552
308.00	5.8964	6.4745	0.8724	0.8739	0.8769	0.8814	0.8873	0.8947	0.9035	0.9137	0.9252
325.00	5.8433	6.4087	0.8571	0.8585	0.8614	0.8657	0.8714	0.8785	0.8869	0.8967	0.9078
334.24	5.8181	6.3776	0.8498	0.8512	0.8541	0.8583	0.8639	0.8708	0.8791	0.8887	0.8996
337.10	5.8108	6.3685	0.8477	0.8491	0.8519	0.8561	0.8617	0.8686	0.8769	0.8864	0.8972
347.00	5.7870	6.3391	0.8409	0.8423	0.8451	0.8492	0.8547	0.8615	0.8695	0.8789	0.8895
351.00	5.7780	6.3280	0.8384	0.8397	0.8425	0.8466	0.8520	0.8588	0.8668	0.8761	0.8866
355.00	5.7093	0.3174	0.8359	0.8373	0.8400	0.8441	0.8495	0.8062	0.8641	0.8734	0.8838
385.15	5.7132	0.2483	0.8200	0.8213	0.8240	0.8279	0.8330	0.8395	0.8471	0.8560	0.8659
407.90	5.0794	6.2008	0.8106	0.8119	0.8144	0.8182	0.8232	0.8295	0.8370	0.8450	0.8553
410.10	5.0087 E 64E2	0.1937	0.8076	0.8088	0.8114	0.8151	0.8201	0.8204	0.8337	0.8423	0.8519
435.90	5 6202	6 1577	0.8011	0.8025	0.8048	0.8085	0.8134	0.8195	0.8250	0.8332	0.8440
441.00	5.0392	6 1270	0.7994	0.8000	0.8031	0.8008	0.8117	0.0170	0.8200	0.0000	0.8427
437.90	5.0251	6 1060	0.7949	0.7902	0.7980	0.8025	0.8071	0.8151	0.8202	0.8264	0.8377
400.00 514.50	5.5970	6.0841	0.7879	0.7891	0.7915	0.7951	0.7998	0.8037	0.8127	0.8208	0.8299
532.00	5 5682	6.0710	0.7328	0.7840	0.7834	0.7860	0.7940	0.3003	0.8072	0.8132	0.8241
546.23	5.5603	6.0613	0.7777	0.7811	0.7834	0.7805	0.7913	0.7913	0.8041	0.8120	0.8184
563.20	5 5516	6.0508	0.7753	0.7765	0.7812	0.7823	0.7868	0.7925	0.3013	0.8050	0.8157
594 10	5 5377	6.0339	0.7716	0.7727	0.7750	0.7625	0.7829	0.7885	0.7952	0.8029	0.8115
611.90	5.5307	6.0253	0.7697	0.7708	0.7731	0.7765	0.7810	0.7865	0.7931	0.8008	0.8094
632.80	5 5232	6.0162	0.7676	0.7688	0.7710	0 7744	0.7789	0 7844	0.7910	0.7986	0.8071
647.10	5.5185	6.0105	0.7664	0.7675	0.7697	0.7731	0.7776	0.7831	0.7896	0.7972	0.8057
670.00	5.5116	6.0022	0.7645	0.7656	0.7679	0.7712	0.7756	0.7811	0.7876	0.7951	0.8036
694.30	5.5051	5.9942	0.7627	0.7639	0.7661	0.7694	0.7738	0.7793	0.7857	0.7932	0.8016
725.00	5.4977	5.9853	0.7608	0.7619	0.7641	0.7674	0.7718	0.7772	0.7836	0.7911	0.7994
754.00	5.4916	5.9779	0.7591	0.7602	0.7624	0.7657	0.7701	0.7755	0.7819	0.7893	0.7976
785.00	5.4858	5.9708	0.7576	0.7587	0.7608	0.7641	0.7685	0.7738	0.7802	0.7876	0.7958
800.00	5.4833	5.9677	0.7569	0.7580	0.7602	0.7634	0.7677	0.7731	0.7795	0.7868	0.7951
836.00	5.4777	5.9610	0.7554	0.7565	0.7586	0.7619	0.7662	0.7715	0.7779	0.7852	0.7934
876.00	5.4723	5.9545	0.7539	0.7550	0.7572	0.7604	0.7647	0.7700	0.7763	0.7836	0.7918
904.00	5.4689	5.9504	0.7530	0.7541	0.7563	0.7595	0.7638	0.7691	0.7754	0.7826	0.7908
911.28	5.4681	5.9494	0.7528	0.7539	0.7561	0.7593	0.7636	0.7688	0.7751	0.7824	0.7905
946.00	5.4645	5.9450	0.7518	0.7529	0.7551	0.7583	0.7625	0.7678	0.7741	0.7813	0.7895
975.00	5.4617	5.9416	0.7511	0.7522	0.7543	0.7575	0.7618	0.7671	0.7733	0.7805	0.7886
1000.00	5.4595	5.9390	0.7505	0.7516	0.7537	0.7569	0.7612	0.7664	0.7727	0.7799	0.7880
1064.00	5.4547	5.9331	0.7492	0.7503	0.7524	0.7556	0.7598	0.7651	0.7713	0.7785	0.7865
1106.00	5.4519	5.9298	0.7485	0.7495	0.7517	0.7549	0.7591	0.7643	0.7705	0.7777	0.7857
1152.00	5.4492	5.9265	0.7478	0.7488	0.7510	0.7541	0.7583	0.7636	0.7697	0.7769	0.7849
1185.00	5.4475	5.9244	0.7473	0.7484	0.7505	0.7537	0.7579	0.7631	0.7693	0.7764	0.7844
1225.00	5.4456	5.9221	0.7468	0.7479	0.7500	0.7531	0.7573	0.7625	0.7687	0.7758	0.7838
1275.00	5.4434	5.9195	0.7462	0.7473	0.7494	0.7526	0.7567	0.7619	0.7681	0.7752	0.7832
1320.00	5.4417	5.9175	0.7458	0.7468	0.7489	0.7521	0.7563	0.7615	0.7676	0.7747	0.7827
Static	5.4179	5.8887	0.7394	0.7405	0.7426	0.7457	0.7498	0.7548	0.7609	0.7678	0.7756

TABLE T1. Mean polarizability matrix elements $\langle \bar{\alpha} \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \bar{\alpha} | \psi_{v',J'} \rangle$ of H₂ for v=0 and v=1.

TABLE T2. Mean polarizability matrix elements	⟨ā	$\langle \rangle_{v,I,v',I'} \equiv \langle \rangle_{v,I,v',I'}$	$\langle \psi_{v,J} $	$ \bar{\alpha} $	$ \psi_{v',J'} $	\rangle of H ₂	for $v=1$	and $v=2$.
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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$											
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\lambda(\text{nm})$	$\langle \bar{\alpha} \rangle_{20,20}$	$\langle \bar{\alpha} \rangle_{20,10}$	$\langle \bar{\alpha} \rangle_{21,11}$	$\langle \bar{\alpha} \rangle_{22,12}$	$\langle \bar{\alpha} \rangle_{23,13}$	$\langle \bar{\alpha} \rangle_{24,14}$	$\langle \bar{\alpha} \rangle_{25,15}$	$\langle \bar{\alpha} \rangle_{26,16}$	$\langle \bar{\alpha} \rangle_{27,17}$	$\langle \bar{\alpha} \rangle_{28,18}$
	182.26	9.0945	1.9519	1.9569	1.9670	1.9821	2.0024	2.0278	2.0584	2.0943	2.1357
	193.00	8.6672	1.8026	1.8069	1.8154	1.8283	1.8454	1.8669	1.8927	1.9229	1.9575
222.4.30 7.9387 1.5601 1.5664 1.5778 1.5883 1.6040 1.6227 1.6466 1.6573 224.30 7.7275 1.4879 1.4908 1.4965 1.5051 1.5165 1.5364 1.5476 1.5673 1.5897 226.00 7.3753 1.3754 1.3826 1.3898 1.3994 1.4131 1.4255 1.4419 1.4606 275.36 7.2261 1.3258 1.3390 1.3454 1.3421 1.3509 1.3351 1.3002 1.4674 308.00 7.0681 1.2285 1.2291 1.2294 1.2309 1.2375 1.2981 1.3013 1.3374 337.0 6.9692 1.2461 1.2571 1.2641 1.2573 1.2785 1.2981 1.2314 31.00 6.9666 1.2211 1.2231 1.2361 1.2614 1.2532 1.2641 1.2533 1.2916 1.2926 1.3323 1.3167 31.00 6.9666 1.2211 1.2310 1.2641 1.2454	213.00	8.1186	1.6165	1.6199	1.6267	1.6369	1.6505	1.6675	1.6879	1.7116	1.7387
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	222.00	7.9387	1.5569	1.5601	1.5664	1.5758	1.5883	1.6040	1.6227	1.6446	1.6694
225.00 7.7275 1.4876 1.4965 1.5061 1.5165 1.5366 1.5476 1.5673 1.5673 226.00 7.3753 1.3754 1.3478 1.3826 1.3898 1.3994 1.4113 1.4285 1.5067 1.5272 226.00 7.2363 1.3287 1.3364 1.3471 1.3739 1.3414 1.4326 2285.00 7.2263 1.3287 1.3391 1.3354 1.3421 1.3590 1.3413 1.3320 1.3343 1.3392 334.24 6.9692 1.2451 1.22651 1.2612 1.2689 1.2785 1.2828 1.3303 1.3178 337.10 6.9522 1.2351 1.2371 1.2409 1.2466 1.2541 1.2634 1.2745 1.2828 1.3313 355.00 6.8956 1.2371 1.2201 1.2328 1.2344 1.2451 1.2659 1.2741 1.2283 1.2341 1.2474 1.2828 1.2341 1.2475 1.2474 1.2286 1.2341 1.2475	224.30	7.8976	1.5434	1.5465	1.5527	1.5619	1.5743	1.5896	1.6080	1.6294	1.6537
248.00 7.558 1.4363 1.4416 1.4495 1.4599 1.4730 1.4886 1.5067 1.5767 226.00 7.3753 1.3774 1.3526 1.3898 1.3399 1.3417 1.3739 1.3853 1.3902 1.4474 285.00 7.2263 1.3287 1.3309 1.3354 1.3421 1.3509 1.3354 1.3421 1.3509 1.3430 1.3430 325.00 7.0073 1.2611 1.2631 1.2671 1.2730 1.2899 1.2023 1.3130 1.3330 1.3341 1.3033 1.3330 1.3341 1.3033 1.3342 1.2662 1.2874 1.2464 1.2498 1.2862 1.2893 1.3104 337.10 6.9586 1.2271 1.2282 1.2371 1.2283 1.2384 1.2459 1.2691 1.2771 1.2282 1.2933 1.3287 1.2873 1.3017 351.00 6.8966 1.2271 1.2280 1.2414 1.2499 1.2691 1.2781 1.2828 1.2814 <td>235.00</td> <td>7.7275</td> <td>1.4879</td> <td>1.4908</td> <td>1.4965</td> <td>1.5051</td> <td>1.5165</td> <td>1.5306</td> <td>1.5476</td> <td>1.5673</td> <td>1.5897</td>	235.00	7.7275	1.4879	1.4908	1.4965	1.5051	1.5165	1.5306	1.5476	1.5673	1.5897
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	248.00	7.5588	1.4336	1.4363	1.4416	1.4495	1.4599	1.4730	1.4886	1.5067	1.5272
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	266.00	7.3753	1.3754	1.3778	1.3826	1.3898	1.3994	1.4113	1.4255	1.4419	1.4606
285.00 7.2263 1.3287 1.3309 1.33421 1.3619 1.3619 1.3751 1.3002 1.4774 308.00 7.0073 1.2611 1.2681 1.2671 1.2730 1.2809 1.2907 1.3023 1.3157 1.3309 334.24 6.9692 1.2495 1.2411 1.2411 1.2514 1.2553 1.2612 1.2689 1.2774 1.2862 1.2903 1.3140 347.00 6.9222 1.2352 1.2371 1.2406 1.2454 1.2451 1.2711 1.2862 1.2933 1.3147 355.00 6.8956 1.2217 1.2200 1.2328 1.2344 1.2458 1.2511 1.2711 1.2828 1.2970 355.00 6.7611 1.1867 1.1884 1.1919 1.1971 1.2023 1.2243 1.2387 1.2454 1.2451 1.2452 1.2444 1.2498 1.2444 1.2293 1.2341 1.2242 1.2466 1.2445 1.2501 1.2174 1.2289 1.2444 407.90 6.7104 1.1716 1.1733 1.1676 1.1717 1.1853 </td <td>275.36</td> <td>7.2971</td> <td>1.3508</td> <td>1.3531</td> <td>1.3578</td> <td>1.3647</td> <td>1.3739</td> <td>1.3853</td> <td>1.3990</td> <td>1.4147</td> <td>1.4326</td>	275.36	7.2971	1.3508	1.3531	1.3578	1.3647	1.3739	1.3853	1.3990	1.4147	1.4326
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	285.00	7.2263	1.3287	1.3309	1.3354	1.3421	1.3509	1.3619	1.3751	1.3902	1.4074
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	308.00	7.0881	1.2859	1.2880	1.2921	1.2984	1.3066	1.3168	1.3290	1.3430	1.3589
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	325.00	7.0073	1.2611	1.2631	1.2671	1.2730	1.2809	1.2907	1.3023	1.3157	1.3309
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	334.24	6.9692	1.2495	1.2514	1.2553	1.2612	1.2689	1.2785	1.2898	1.3030	1.3178
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	337.10	6.9581	1.2461	1.2481	1.2519	1.2577	1.2654	1.2749	1.2862	1.2993	1.3140
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	347.00	6.9222	1.2352	1.2371	1.2409	1.2466	1.2541	1.2634	1.2745	1.2873	1.3017
355.00 6.8956 1.2271 1.2290 1.2328 1.2384 1.2485 1.2283 1.2387 1.2506 1.2764 1.2291 416.10 6.7451 1.1867 1.1884 1.1919 1.1971 1.2039 1.2124 1.2225 1.2341 1.2424 416.10 6.7451 1.1867 1.1873 1.1766 1.1817 1.1833 1.1666 1.2063 1.2174 1.2289 1.2302 441.60 6.7015 1.1689 1.1706 1.1740 1.1790 1.1863 1.1988 1.2063 1.2174 1.2289 457.90 6.6776 1.1618 1.1676 1.1817 1.1883 1.1863 1.1959 1.2069 1.2193 488.00 6.6400 1.1507 1.1523 1.1556 1.1604 1.1662 1.1754 1.1859 1.198 1.2069 1.2069 1.2193 546.23 6.567 1.1380 1.1395 1.1427 1.1474 1.1551 1.167 1.1667 1.1771 1.1886 546.23 6.5520 1.1248 1.1264 1.1294 1.1400	351.00	6.9086	1.2311	1.2330	1.2368	1.2424	1.2498	1.2591	1.2701	1.2828	1.2970
335.15 6.8114 1.2018 1.2036 1.2071 1.2125 1.2285 1.2283 1.2387 1.2606 1.2641 407.90 6.7611 1.1819 1.1837 1.1871 1.1922 1.1900 1.2074 1.2174 1.2285 1.2341 1.2472 416.00 6.7104 1.1716 1.1733 1.1766 1.1817 1.1833 1.1966 1.2063 1.2174 1.2289 1.2342 441.60 6.7104 1.1716 1.1733 1.1766 1.1817 1.1838 1.1959 1.2069 1.2123 488.00 6.6400 1.1507 1.1628 1.2041 1.2069 1.2173 542.00 6.6526 1.1426 1.1442 1.1474 1.5236 1.1613 1.1809 1.1926 546.23 6.5551 1.1345 1.1361 1.1392 1.1439 1.1501 1.1577 1.1667 1.1730 1.1848 611.90 6.5421 1.1203 1.1244 1.1309 1.1400 1.1475 1.1564 1.1633 1.1746 611.90 6.520 1.1248	355.00	6.8956	1.2271	1.2290	1.2328	1.2384	1.2458	1.2549	1.2659	1.2784	1.2926
407.90 6.7611 1.1867 1.1884 1.1919 1.1971 1.2039 1.2124 1.2225 1.2341 1.2472 416.10 6.7014 1.1716 1.1733 1.1766 1.1817 1.1883 1.1966 1.2063 1.2176 1.2302 441.60 6.7015 1.1689 1.1706 1.1740 1.1790 1.1856 1.1938 1.2063 1.2147 1.2272 457.90 6.6776 1.1618 1.1653 1.1668 1.1747 1.1840 1.1948 1.2069 514.50 6.6126 1.1426 1.1444 1.1534 1.1668 1.1747 1.1840 1.1948 1.2069 546.23 6.5851 1.1336 1.1323 1.1354 1.1401 1.1452 1.1538 1.667 1.1771 1.1888 563.20 6.5723 1.1308 1.1323 1.1354 1.1401 1.1462 1.1538 1.1667 1.1771 1.1886 611.90 6.5417 1.1218 1.2231 1.233 1.264 1.309 1.3469 1.4444 1.1532 1.1653 1.1770	385.15	6.8114	1.2018	1.2036	1.2071	1.2125	1.2195	1.2283	1.2387	1.2506	1.2641
416.10 6.7451 1.1819 1.1871 1.1922 1.1990 1.2074 1.2174 1.2289 1.2418 435.96 6.7105 1.1689 1.1706 1.1740 1.1790 1.1856 1.1938 1.2055 1.2176 1.2322 457.90 6.6776 1.1618 1.1635 1.1668 1.1717 1.1856 1.1983 1.1959 1.2069 1.213 488.00 6.6400 1.1426 1.1442 1.1474 1.1521 1.1584 1.1662 1.1754 1.1859 1.1998 542.00 6.5851 1.1345 1.1361 1.1392 1.1439 1.1501 1.1577 1.1667 1.1771 1.1888 563.20 6.5520 1.1248 1.1264 1.1294 1.1309 1.1369 1.1444 1.1532 1.1663 1.1780 611.90 6.5417 1.1218 1.1223 1.1244 1.1309 1.1369 1.1444 1.1532 1.1633 1.1766 677.00 6.5329 1.1166 1.1211 1.1256 1.1316 1.1389 1.1476 1.1576 1.688	407.90	6.7611	1.1867	1.1884	1.1919	1.1971	1.2039	1.2124	1.2225	1.2341	1.2472
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	416.10	6.7451	1.1819	1.1837	1.1871	1.1922	1.1990	1.2074	1.2174	1.2289	1.2418
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	435.96	6.7104	1.1716	1.1733	1.1766	1.1817	1.1883	1.1966	1.2063	1.2176	1.2302
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	441.60	6.7015	1.1689	1.1706	1.1740	1.1790	1.1856	1.1938	1.2035	1.2147	1.2272
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	457.90	6.6776	1.1618	1.1635	1.1668	1.1717	1.1783	1.1863	1.1959	1.2069	1.2193
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	488.00	6.6400	1.1507	1.1523	1.1556	1.1604	1.1668	1.1747	1.1840	1.1948	1.2069
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	514.50	6.6126	1.1426	1.1442	1.1474	1.1521	1.1584	1.1662	1.1754	1.1859	1.1978
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	532.00	6.5967	1.1380	1.1395	1.1427	1.1474	1.1536	1.1613	1.1704	1.1809	1.1926
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	546.23	6.5851	1.1345	1.1361	1.1392	1.1439	1.1501	1.1577	1.1667	1.1771	1.1888
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	563.20	6.5723	1.1308	1.1323	1.1354	1.1401	1.1462	1.1538	1.1627	1.1730	1.1846
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	594.10	6.5520	1.1248	1.1264	1.1294	1.1340	1.1400	1.1475	1.1564	1.1665	1.1780
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	611.90	6.5417	1.1218	1.1233	1.1264	1.1309	1.1369	1.1444	1.1532	1.1633	1.1746
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	632.80	6.5307	1.1186	1.1201	1.1231	1.1277	1.1336	1.1410	1.1497	1.1598	1.1710
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	647.10	6.5239	1.1166	1.1181	1.1211	1.1256	1.1316	1.1389	1.1476	1.1576	1.1688
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	670.00	6.5138	1.1137	1.1152	1.1182	1.1226	1.1285	1.1358	1.1445	1.1544	1.1655
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	694.30	6.5042	1.1109	1.1124	1.1153	1.1198	1.1256	1.1329	1.1415	1.1514	1.1624
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	725.00	6.4935	1.1077	1.1092	1.1122	1.1166	1.1224	1.1296	1.1382	1.1480	1.1589
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	754.00	6.4846	1.1052	1.1066	1.1096	1.1140	1.1198	1.1269	1.1354	1.1451	1.1561
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	785.00	6.4762	1.1027	1.1042	1.1071	1.1115	1.1172	1.1244	1.1328	1.1425	1.1533
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	800.00	6.4725	1.1016	1.1031	1.1060	1.1104	1.1161	1.1232	1.1316	1.1413	1.1521
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	836.00	6.4644	1.0993	1.1007	1.1036	1.1080	1.1137	1.1208	1.1291	1.1387	1.1495
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	876.00	6.4565	1.0970	1.0984	1.1013	1.1056	1.1113	1.1184	1.1267	1.1363	1.1470
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	904.00	6.4517	1.0956	1.0970	1.0999	1.1042	1.1099	1.1169	1.1252	1.1347	1.1454
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	911.28	6.4505	1.0952	1.0967	1.0996	1.1038	1.1095	1.1165	1.1248	1.1344	1.1450
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	946.00	6.4452	1.0937	1.0951	1.0980	1.1023	1.1079	1.1149	1.1232	1.1327	1.1433
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	975.00	6.4412	1.0925	1.0940	1.0968	1.1011	1.1067	1.1137	1.1220	1.1314	1.1420
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1000.00	6.4380	1.0916	1.0930	1.0959	1.1002	1.1058	1.1128	1.1210	1.1304	1.1410
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1064.00	6.4309	1.0896	1.0910	1.0938	1.0981	1.1037	1.1106	1.1188	1.1282	1.1387
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1106.00	6.4269	1.0884	1.0898	1.0927	1.0969	1.1025	1.1094	1.1176	1.1269	1.1374
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1152.00	6.4230	1.0873	1.0887	1.0915	1.0958	1.1013	1.1082	1.1164	1.1257	1.1362
1225.00 6.4178 1.0858 1.0872 1.0900 1.0942 1.0998 1.1066 1.1147 1.1241 1.1345 1275.00 6.4147 1.0849 1.0863 1.0891 1.0933 1.0988 1.1057 1.1138 1.1231 1.1335 1320.00 6.4122 1.0841 1.0856 1.0884 1.0926 1.0981 1.1049 1.1130 1.1223 1.1327 Static 6.3778 1.0742 1.0756 1.0783 1.0824 1.0879 1.0946 1.1025 1.1115 1.1217	1185.00	6.4205	1.0866	1.0880	1.0908	1.0950	1.1006	1.1075	1.1156	1.1249	1.1354
1275.00 0.4147 1.0849 1.0863 1.0891 1.0933 1.0988 1.1057 1.1138 1.1231 1.1335 1320.00 6.4122 1.0841 1.0856 1.0884 1.0926 1.0981 1.1049 1.1130 1.1223 1.1327 Static 6.3778 1.0742 1.0756 1.0783 1.0824 1.0879 1.0946 1.1025 1.1115 1.1217	1225.00	6.4178	1.0858	1.0872	1.0900	1.0942	1.0998	1.1066	1.1147	1.1241	1.1345
1320.00 0.4122 1.0841 1.0856 1.0884 1.0926 1.0981 1.1049 1.1130 1.1223 1.1327 Static 6.3778 1.0742 1.0756 1.0783 1.0824 1.0879 1.0946 1.1025 1.1115 1.1217	1275.00	6.4147	1.0849	1.0863	1.0891	1.0933	1.0988	1.1057	1.1138	1.1231	1.1335
Static 6.3778 1.0742 1.0756 1.0783 1.0824 1.0879 1.0946 1.1025 1.1115 1.1217	1320.00	6.4122	1.0841	1.0856	1.0884	1.0926	1.0981	1.1049	1.1130	1.1223	1.1327
	Static	6.3778	1.0742	1.0756	1.0783	1.0824	1.0879	1.0946	1.1025	1.1115	1.1217

TABLE T3. Mean polarizability matrix elements $\langle \bar{\alpha} \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \bar{\alpha} | \psi_{v',J'} \rangle$ of HD for v=0 and v=1.

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$\lambda(\text{nm})$	$\langle \bar{lpha} angle_{00,00}$	$\langle \bar{\alpha} \rangle_{10,10}$	$\langle \bar{\alpha} \rangle_{10,00}$	$\langle \bar{\alpha} \rangle_{11,01}$	$\langle \bar{\alpha} \rangle_{12,02}$	$\langle \bar{\alpha} \rangle_{13,03}$	$\langle \bar{\alpha} \rangle_{14,04}$	$\langle \bar{\alpha} \rangle_{15,05}$	$\langle \bar{\alpha} \rangle_{16,06}$	$\langle \bar{\alpha} \rangle_{17,07}$	$\langle \bar{\alpha} \rangle_{18,08}$
182.26	7.0472	7.8390	1.1662	1.1684	1.1728	1.1794	1.1883	1.1995	1.2128	1.2285	1.2466
193.00	6.8114	7.5362	1.0888	1.0907	1.0946	1.1004	1.1081	1.1178	1.1295	1.1431	1.1587
213.00	6.4949	7.1368	0.9899	0.9915	0.9947	0.9995	1.0058	1.0138	1.0233	1.0345	1.0472
222.00	6.3877	7.0032	0.9577	0.9591	0.9621	0.9666	0.9725	0.9800	0.9889	0.9993	1.0111
224.30	6.3630	6.9725	0.9503	0.9518	0.9547	0.9591	0.9649	0.9723	0.9810	0.9912	1.0029
235.00	6.2598	6.8448	0.9200	0.9213	0.9241	0.9282	0.9337	0.9405	0.9487	0.9582	0.9691
248.00	6.1559	6.7170	0.8900	0.8913	0.8938	0.8977	0.9028	0.9092	0.9168	0.9257	0.9358
266.00	6.0412	6.5767	0.8576	0.8588	0.8611	0.8647	0.8694	0.8753	0.8824	0.8905	0.8999
275.36	5.9918	6.5166	0.8438	0.8450	0.8473	0.8507	0.8553	0.8610	0.8678	0.8757	0.8847
285.00	5.9467	6.4619	0.8314	0.8325	0.8347	0.8381	0.8425	0.8480	0.8546	0.8622	0.8709
308.00	5.8581	6.3546	0.8073	0.8083	0.8104	0.8135	0.8177	0.8228	0.8290	0.8362	0.8443
325.00	5.8057	6.2915	0.7932	0.7942	0.7962	0.7992	0.8032	0.8082	0.8141	0.8210	0.8289
334.24	5.7810	6.2617	0.7866	0.7876	0.7895	0.7925	0.7964	0.8013	0.8072	0.8139	0.8216
337.10	5.7737	6.2531	0.7847	0.7856	0.7876	0.7906	0.7945	0.7993	0.8051	0.8119	0.8195
347.00	5.7503	6.2249	0.7784	0.7794	0.7813	0.7842	0.7881	0.7928	0.7985	0.8052	0.8127
351.00	5.7414	6.2142	0.7761	0.7771	0.7790	0.7818	0.7857	0.7904	0.7961	0.8026	0.8101
355.00	5.7329	6.2040	0.7738	0.7748	0.7767	0.7796	0.7833	0.7881	0.7937	0.8002	0.8076
385.15	5.6776	6.1377	0.7593	0.7602	0.7621	0.7648	0.7684	0.7730	0.7784	0.7846	0.7917
407.90	5.6443	6.0979	0.7507	0.7516	0.7533	0.7560	0.7596	0.7640	0.7692	0.7753	0.7822
416.10	5.6337	6.0853	0.7479	0.7488	0.7506	0.7532	0.7568	0.7611	0.7663	0.7724	0.7792
435.96	5.6106	6.0578	0.7420	0.7428	0.7446	0.7472	0.7506	0.7549	0.7601	0.7660	0.7727
441.60	5.6047	6.0507	0.7404	0.7413	0.7430	0.7456	0.7491	0.7534	0.7585	0.7644	0.7711
457.90	5.5888	6.0317	0.7364	0.7372	0.7389	0.7415	0.7449	0.7491	0.7541	0.7600	0.7666
488.00	5.5637	6.0019	0.7299	0.7308	0.7325	0.7350	0.7383	0.7424	0.7474	0.7531	0.7596
514.50	5.5453	5.9800	0.7253	0.7261	0.7277	0.7302	0.7335	0.7376	0.7425	0.7481	0.7545
532.00	5.5347	5.9674	0.7226	0.7234	0.7250	0.7275	0.7307	0.7348	0.7396	0.7452	0.7515
546.23	5.5268	5.9581	0.7206	0.7214	0.7230	0.7255	0.7287	0.7327	0.7375	0.7431	0.7494
563.20	5.5183	5.9479	0.7184	0.7192	0.7208	0.7233	0.7265	0.7305	0.7352	0.7408	0.7470
594.10	5.5046	5.9317	0.7149	0.7157	0.7174	0.7197	0.7229	0.7269	0.7316	0.7371	0.7432
611.90	5.4977	5.9235	0.7132	0.7140	0.7156	0.7180	0.7211	0.7251	0.7298	0.7352	0.7413
632.80	5.4903	5.9147	0.7113	0.7121	0.7137	0.7161	0.7192	0.7231	0.7278	0.7332	0.7393
647.10	5.4856	5.9092	0.7102	0.7110	0.7125	0.7149	0.7180	0.7219	0.7266	0.7320	0.7380
670.00	5.4788	5.9012	0.7085	0.7093	0.7108	0.7132	0.7163	0.7202	0.7248	0.7301	0.7362
694.30	5.4724	5.8935	0.7068	0.7076	0.7092	0.7115	0.7146	0.7185	0.7231	0.7284	0.7344
725.00	5.4651	5.8849	0.7050	0.7058	0.7074	0.7097	0.7128	0.7166	0.7212	0.7265	0.7324
754.00	5.4591	5.8778	0.7035	0.7043	0.7058	0.7082	0.7112	0.7150	0.7196	0.7248	0.7308
785.00	5.4534	5.8710	0.7021	0.7029	0.7044	0.7067	0.7098	0.7136	0.7181	0.7233	0.7292
800.00	5.4509	5.8681	0.7015	0.7022	0.7038	0.7061	0.7091	0.7129	0.7174	0.7226	0.7286
836.00	5.4454	5.8616	0.7001	0.7009	0.7024	0.7047	0.7077	0.7115	0.7160	0.7212	0.7271
876.00	5.4401	5.8553	0.6988	0.6995	0.7011	0.7033	0.7064	0.7101	0.7146	0.7198	0.7256
904.00	5.4368	5.8514	0.6979	0.6987	0.7002	0.7025	0.7055	0.7093	0.7137	0.7189	0.7247
911.28	5.4360	5.8504	0.6977	0.6985	0.7000	0.7023	0.7053	0.7091	0.7135	0.7187	0.7245
946.00	5.4324	5.8461	0.6968	0.6976	0.6991	0.7014	0.7044	0.7081	0.7126	0.7177	0.7235
975.00	5.4296	5.8429	0.6962	0.6969	0.6984	0.7007	0.7037	0.7074	0.7119	0.7170	0.7228
1000.00	5.4275	5.8404	0.6956	0.6964	0.6979	0.7002	0.7032	0.7069	0.7113	0.7164	0.7222
1064.00	5.4227	5.8347	0.6944	0.6952	0.6967	0.6989	0.7019	0.7056	0.7100	0.7151	0.7209
1106.00	5.4199	5.8315	0.6938	0.6945	0.6960	0.6983	0.7012	0.7049	0.7093	0.7144	0.7202
1152.00	5.4173	5.8284	0.6931	0.6939	0.6954	0.6976	0.7006	0.7043	0.7086	0.7137	0.7195
1185.00	5.4156	5.8264	0.6927	0.6934	0.6949	0.6972	0.7001	0.7038	0.7082	0.7133	0.7190
1225.00	5.4137	5.8241	0.6922	0.6930	0.6945	0.6967	0.6997	0.7033	0.7077	0.7128	0.7185
1275.00	5 4116	5 8216	0.6917	0.6924	0.6939	0.6962	0.6991	0.7028	0 7072	0 7122	0 7179
1320.00	5 4099	5 8196	0.6913	0.6920	0.6935	0.6957	0.6987	0.7024	0.7067	0 7118	0.7175
Static	5 3864	5 7010	0.6855	0.6862	0.6877	0.6800	0.6928	0.6964	0.7006	0 7056	0 7119
Static	0.0004	0.1919	0.0000	0.0002	0.0017	0.0055	0.0528	0.0504	0.7000	0.1000	0.1112

TABLE T4. Mean polarizability matrix elements $\langle \bar{\alpha} \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \bar{\alpha} | \psi_{v',J'} \rangle$ of HD for v=1 and v=2.

λ (nm)	$\langle \bar{\alpha} \rangle_{20,20}$	$(\bar{\alpha})_{20,10}$	(ā) 21.11	(ā)22.12	$\langle \bar{\alpha} \rangle_{22,12}$	$\langle \bar{\alpha} \rangle_{24,14}$	$\langle \bar{\alpha} \rangle_{25,15}$	$\langle \bar{\alpha} \rangle_{26,16}$	$\langle \bar{\alpha} \rangle_{27,17}$	$\langle \bar{\alpha} \rangle_{28,18}$
199.96	(a/20,20	1.7750	1 7794	1 7959	1 7055	1 8002	1 9964	1.9479	1.9714	1 2002
102.20	8.1221	1.7730	1.7764	1.7652	1.7900	1.6092	1.6204	1.0472	1.0714	1.6995
212.00	7 9999	1.0439	1.0408	1.0527	1 4025	1.6732	1.0070	1.7033	1.7201	1.7497
213.00	7.6526	1.4795	1.4017	1.4004	1.4935	1.3029	1.3140	1.5267	1.0401	1.5038
222.00	7.60072	1.4204	1.4280	1.4330	1.4395	1.4482	1.4591	1.4721	1.4872	1.5045
224.30	7.6293	1.4144	1.4100	1.4208	1.4273	1.4358	1.4405	1.4593	1.4741	1.4911
233.00	7 2160	1.3030	1.3070	1.3710	1.3709	1.3649	1.3947	1.4000	1.4203 1.2677	1.4300
248.00	7.5100	1.5105	1.5164	1.5221	1.5270	1.3349	1.3440	1.5550	1.3077	1.3021
266.00	7.1400	1.2044	1.2001	1.2095	1.2745	1.2812	1.2890	1.2996	1.3112	1.3244
275.30	7.0728	1.2424	1.2440	1.2473	1.2021	1.2080	1.2000	1.2703	1.2874	1.3001
285.00	7.0069	1.2220	1.2241	1.2273	1.2320	1.2382	1.2460	1.2002	1.2000	1.2782
308.00	0.8780	1.1842	1.1800	1.1885	1.1929	1.1987	1.2060	1.2140	1.2240	1.2359
325.00	6.8025	1.1619	1.1633	1.1661	1.1703	1.1758	1.1828	1.1910	1.2006	1.2114
334.24	6.7669	1.1514	1.1528	1.1555	1.1596	1.1651	1.1719	1.1800	1.1894	1.2000
337.10	6.7565	1.1484	1.1497	1.1525	1.1566	1.1620	1.1687	1.1768	1.1861	1.1967
347.00	6.7229	1.1386	1.1399	1.1426	1.1466	1.1519	1.1585	1.1664	1.1755	1.1859
351.00	6.7102	1.1349	1.1362	1.1388	1.1428	1.1481	1.1547	1.1625	1.1716	1.1818
355.00	6.6980	1.1313	1.1326	1.1353	1.1392	1.1445	1.1510	1.1588	1.1678	1.1779
385.15	6.6192	1.1084	1.1097	1.1122	1.1160	1.1210	1.1273	1.1347	1.1433	1.1530
407.90	6.5720	1.0948	1.0961	1.0985	1.1022	1.1071	1.1131	1.1203	1.1287	1.1381
416.10	6.5570	1.0905	1.0918	1.0942	1.0978	1.1027	1.1087	1.1158	1.1241	1.1334
435.96	6.5245	1.0812	1.0824	1.0848	1.0884	1.0931	1.0990	1.1060	1.1141	1.1232
441.60	6.5161	1.0788	1.0800	1.0824	1.0859	1.0907	1.0965	1.1035	1.1115	1.1206
457.90	6.4936	1.0724	1.0736	1.0759	1.0794	1.0841	1.0899	1.0967	1.1047	1.1136
488.00	6.4584	1.0624	1.0635	1.0658	1.0693	1.0738	1.0794	1.0862	1.0939	1.1027
514.50	6.4326	1.0551	1.0562	1.0585	1.0618	1.0663	1.0719	1.0785	1.0861	1.0947
532.00	6.4177	1.0509	1.0520	1.0542	1.0576	1.0620	1.0675	1.0741	1.0816	1.0902
546.23	6.4067	1.0478	1.0489	1.0511	1.0544	1.0588	1.0643	1.0708	1.0783	1.0868
563.20	6.3947	1.0444	1.0455	1.0477	1.0510	1.0554	1.0608	1.0672	1.0747	1.0831
594.10	6.3756	1.0390	1.0401	1.0423	1.0455	1.0498	1.0552	1.0616	1.0689	1.0772
611.90	6.3659	1.0363	1.0373	1.0395	1.0427	1.0470	1.0524	1.0587	1.0660	1.0743
632.80	6.3556	1.0334	1.0344	1.0366	1.0398	1.0441	1.0494	1.0557	1.0629	1.0711
647.10	6.3492	1.0315	1.0326	1.0348	1.0380	1.0422	1.0475	1.0538	1.0610	1.0692
670.00	6.3397	1.0289	1.0300	1.0321	1.0353	1.0395	1.0447	1.0510	1.0582	1.0663
694.30	6.3307	1.0264	1.0274	1.0295	1.0327	1.0369	1.0421	1.0483	1.0555	1.0635
725.00	6.3206	1.0235	1.0246	1.0267	1.0299	1.0340	1.0392	1.0454	1.0525	1.0605
754.00	6.3123	1.0212	1.0222	1.0243	1.0275	1.0316	1.0368	1.0429	1.0500	1.0579
785.00	6.3043	1.0190	1.0200	1.0221	1.0252	1.0294	1.0345	1.0406	1.0476	1.0555
800.00	6.3008	1.0180	1.0190	1.0211	1.0242	1.0284	1.0335	1.0395	1.0465	1.0544
836.00	6.2932	1.0159	1.0169	1.0190	1.0221	1.0262	1.0313	1.0373	1.0443	1.0521
876.00	6.2858	1.0138	1.0148	1.0169	1.0200	1.0241	1.0291	1.0351	1.0421	1.0499
904.00	6.2812	1.0125	1.0136	1.0156	1.0187	1.0228	1.0278	1.0338	1.0407	1.0485
911.28	6.2801	1.0122	1.0132	1.0153	1.0184	1.0224	1.0275	1.0335	1.0404	1.0482
946.00	6.2751	1.0108	1.0119	1.0139	1.0170	1.0210	1.0260	1.0320	1.0389	1.0467
975.00	6.2713	1.0098	1.0108	1.0128	1.0159	1.0199	1.0249	1.0309	1.0378	1.0455
1000.00	6.2684	1.0089	1.0100	1.0120	1.0151	1.0191	1.0241	1.0300	1.0369	1.0446
1064.00	6.2617	1.0071	1.0081	1.0101	1.0132	1.0172	1.0222	1.0281	1.0349	1.0426
1106.00	6.2579	1.0060	1.0071	1.0091	1.0121	1.0161	1.0211	1.0270	1.0338	1.0415
1152.00	6.2543	1.0050	1.0060	1.0081	1.0111	1.0151	1.0200	1.0259	1.0327	1.0404
1185.00	6.2519	1.0044	1.0054	1.0074	1.0104	1.0144	1.0193	1.0252	1.0320	1.0397
1225.00	6.2493	1.0036	1.0047	1.0067	1.0097	1.0137	1.0186	1.0245	1.0312	1.0389
1275.00	6.2464	1.0028	1.0038	1.0058	1.0089	1.0128	1.0178	1.0236	1.0304	1.0380
1320.00	6.2440	1.0022	1.0032	1.0052	1.0082	1.0122	1.0171	1.0229	1.0297	1.0373
Static	6.2116	0.9932	0.9942	0.9961	0.9991	1.0030	1.0078	1.0135	1.0201	1.0275

TABLE T5. Mean polarizability matrix elements $\langle \bar{\alpha} \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \bar{\alpha} | \psi_{v',J'} \rangle$ of D₂ for v=0 and v=1.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$,					
	$\lambda(\text{nm})$	$\langle \bar{lpha} angle_{00,00}$	$\langle \bar{\alpha} \rangle_{10,10}$	$\langle \bar{\alpha} \rangle_{10,00}$	$\langle \bar{\alpha} \rangle_{11,01}$	$\langle \bar{\alpha} \rangle_{12,02}$	$\langle \bar{\alpha} \rangle_{13,03}$	$\langle \bar{\alpha} \rangle_{14,04}$	$\langle \bar{\alpha} \rangle_{15,05}$	$\langle \bar{\alpha} \rangle_{16,06}$	$\langle \bar{\alpha} \rangle_{17,07}$	$\langle \bar{\alpha} \rangle_{18,08}$
193.00 6.7466 7.3281 0.9722 0.9733 0.9781 0.9897 0.9844 0.9064 1.0014 1.0137 222.00 6.3323 6.8279 0.8571 0.8580 0.8580 0.8525 0.8600 0.8775 0.8768 0.8822 0.8333 0.8610 0.8752 0.8822 223.00 6.3015 6.7875 0.7875 0.7878 0.8724 0.8522 0.8322 0.8333 0.8410 0.8460 0.8535 246.00 6.1052 6.5757 0.7785 0.7760 0.7711 0.7776 0.7781 0.7796 0.7839 0.7888 0.7465 275.36 5.9442 6.3681 0.7465 0.7748 0.7492 0.7373 0.7339 0.7376 0.7420 0.7474 326.00 5.5130 6.5145 0.7124 0.7124 0.7141 0.7114 0.7112 0.7164 0.7137 0.7122 0.7724 337.10 5.7302 6.1164 0.7045 0.7076 0.7111 0.7112	182.26	6.9768	7.6104	1.0398	1.0411	1.0437	1.0477	1.0529	1.0595	1.0674	1.0767	1.0873
212.00 6.4372 6.9556 0.8854 0.8854 0.8592 0.8957 0.9054 0.9121 0.9197 222.00 6.3081 6.7990 0.8506 0.8558 0.8559 0.8594 0.8583 0.8691 0.8752 0.8822 223.00 6.2076 6.7578 0.8293 0.8224 0.8229 0.8322 0.8363 0.8412 0.8460 0.8532 248.00 6.1052 6.5578 0.7795 0.7788 0.7796 0.7789 0.7789 0.7789 0.7788 0.7798 0.7798 0.7798 0.7798 0.7798 0.7798 0.7798 0.7798 0.7798 0.7798 0.7798 0.7378 0.7858 0.7493 0.7478 0.7478 0.7749 0.7379 0.7378 0.7858 0.7398 0.7376 0.783 0.7863 0.7469 0.7420 0.7469 0.7490 0.7315 0.7768 0.7370 0.7370 0.7370 0.7370 0.7370 0.7370 0.7509 0.7114 0.7112 0.7152 <td< td=""><td>193.00</td><td>6.7466</td><td>7.3281</td><td>0.9722</td><td>0.9733</td><td>0.9756</td><td>0.9791</td><td>0.9837</td><td>0.9894</td><td>0.9964</td><td>1.0044</td><td>1.0137</td></td<>	193.00	6.7466	7.3281	0.9722	0.9733	0.9756	0.9791	0.9837	0.9894	0.9964	1.0044	1.0137
222.30 6.3223 6.8279 0.8571 0.8580 0.8529 0.8560 0.8705 0.8753 0.8822 235.00 6.2070 6.6785 0.8239 0.8248 0.8244 0.8249 0.8322 0.8363 0.8412 0.8460 0.8532 248.00 6.1052 6.5785 0.7975 0.7988 0.7669 0.7661 0.77761 0.7736 0.7888 0.7468 0.7469 0.7669 0.7637 0.77761 0.7738 0.7788 0.7420 0.7440 0.7420 0.7440 0.7420 0.7440 0.7420 0.7440 0.7241 0.7712 0.77120 0.7720 0.7333 0.7386 0.7740 0.7240 0.7469 331.24 5.7372 6.1126 0.7045 0.7061 0.7097 0.71121 0.71121 0.71121 0.71121 0.71121 0.71133 0.7162 0.7148 0.7224 0.7224 0.7224 0.7245 0.7104 0.7075 0.71130 0.7112 0.71131 0.7125 0.7114 0.71133 <td>213.00</td> <td>6.4372</td> <td>6.9536</td> <td>0.8854</td> <td>0.8864</td> <td>0.8883</td> <td>0.8912</td> <td>0.8950</td> <td>0.8997</td> <td>0.9054</td> <td>0.9121</td> <td>0.9197</td>	213.00	6.4372	6.9536	0.8854	0.8864	0.8883	0.8912	0.8950	0.8997	0.9054	0.9121	0.9197
223.00 6.3081 6.7990 0.8506 0.8515 0.8529 0.8594 0.8638 0.8612 0.8469 0.8535 248.00 6.1052 6.5578 0.7975 0.7983 0.7980 0.8229 0.8322 0.8363 0.8412 0.7889 0.8251 266.00 5.9947 6.4251 0.7688 0.7757 0.7589 0.7761 0.7761 0.7761 0.7761 0.7761 0.7781 0.7781 0.7761 0.7783 0.7761 0.7781 0.7781 0.7781 0.7742 0.7761 0.7741 0.7742 0.7741 0.7289 0.7337 333.00 5.7372 6.1262 0.7062 0.7068 0.7080 0.7097 0.7111 0.7210 0.7228 0.7337 331.00 5.7071 6.0911 0.6995 0.7007 0.7027 0.7056 0.7104 0.7133 0.7160 0.7130 0.7170 351.00 5.66906 6.0713 0.6995 0.6972 0.6773 0.6798 0.6824 0.6864<	222.00	6.3323	6.8279	0.8571	0.8580	0.8598	0.8625	0.8660	0.8705	0.8758	0.8820	0.8892
235.00 6.2070 6.6785 0.2823 0.8248 0.8242 0.8222 0.8363 0.8412 0.8460 248.00 6.1052 6.578 0.7795 0.7798 0.7784 0.7796 0.7888 0.7764 275.36 5.99427 6.4251 0.7458 0.7458 0.7699 0.7637 0.7761 0.7712 0.77760 0.7815 285.00 5.9900 6.3163 0.7458 0.7244 0.7212 0.7728 0.7337 0.7338 0.7760 0.7333 0.7740 0.7228 0.7333 0.7140 0.7212 0.7214 0.7211 0.7211 0.7211 0.7213 0.7228 0.7333 0.7160 0.7210 0.7214 0.7213 0.7152 0.7198 0.7121 0.7112 0.7112 0.7112 0.7112 0.7112 0.7123 0.7164 0.7214 0.7213 0.7214 0.7214 0.7213 0.7164 0.7072 0.7112 0.7112 0.7112 0.7112 0.7112 0.7112 0.7113 0.7149 <	224.30	6.3081	6.7990	0.8506	0.8515	0.8533	0.8559	0.8594	0.8638	0.8691	0.8752	0.8822
248.00 6.1052 6.5578 0.7975 0.7983 0.7998 0.8021 0.8052 0.8011 0.8136 0.8136 0.8136 0.8136 0.71845 2256.00 5.9442 6.3681 0.7558 0.7575 0.7589 0.7637 0.7721 0.77712 0.77760 0.7713 325.00 5.8130 6.2145 0.7214 0.7224 0.7325 0.7336 0.7376 0.7242 0.7337 334.24 5.7372 6.1262 0.7068 0.7080 0.7097 0.7114 0.7116 0.7216 0.7216 0.7216 0.7216 0.7216 0.7216 0.7216 0.7216 0.7216 0.7216 0.7112 0.7156 0.7236 0.7496 0.7035 0.7069 0.7106 0.7112 0.7152 0.7184 0.7216 0.7112 0.7152 0.7176 0.7130 0.7112 0.7122 0.7133 0.7109 0.7134 0.7109 0.7134 0.7769 0.8814 0.8914 0.8934 0.8934 0.8934 0.8934	235.00	6.2070	6.6785	0.8239	0.8248	0.8264	0.8289	0.8322	0.8363	0.8412	0.8469	0.8535
266.00 5.9927 6.4251 0.7696 0.7711 0.7724 0.7761 0.7739 0.77839 0.7839 0.7815 275.36 5.9000 6.3163 0.7458 0.7475 0.77518 0.7558 0.7558 0.7598 0.7464 0.7469 308.00 5.7616 6.1545 0.7124 0.7248 0.7307 0.7333 0.7176 0.7242 0.72248 0.72474 334.24 5.7372 6.1180 0.7045 0.7063 0.7090 0.7113 0.7169 0.7224 0.72289 0.7334 347.00 5.7071 6.0110 0.6999 0.6995 0.7007 0.7014 0.7109 0.7113 0.7164 355.00 5.6096 6.0113 0.6949 0.6955 0.6986 0.7004 0.7025 0.7030 0.7144 0.7149 0.7154 355.00 5.60356 6.0292 5.9733 0.6744 0.6749 0.6874 0.6879 0.6831 0.6868 0.6933 407.90 5.6356	248.00	6.1052	6.5578	0.7975	0.7983	0.7998	0.8021	0.8052	0.8091	0.8136	0.8190	0.8251
275.36 5.9442 6.3681 0.7575 0.7579 0.7589 0.7697 0.7711 0.7712 0.7712 0.7712 0.7712 0.7697 328.00 5.8130 6.2145 0.7215 0.7224 0.7224 0.7325 0.7336 0.7376 0.7420 0.7433 334.44 5.7372 6.1262 0.7068 0.7080 0.7080 0.7181 0.7114 0.7118 0.7218 0.7228 0.7237 337.10 5.7372 6.180 0.7045 0.7065 0.7069 0.7124 0.7181 0.7118 0.7218 0.7228 0.7234 351.00 5.6984 6.0810 0.69690 0.6975 0.7097 0.7025 0.7066 0.7090 0.7112 0.7156 0.7122 0.7183 351.00 5.6984 6.0810 0.69694 0.6976 0.7076 0.7069 0.7069 0.7112 0.7124 0.7164 0.7133 0.7799 0.6834 0.6856 0.6894 0.6974 0.6773 0.6779 0.6840 0.6840 0.6894 0.6994 0.6979 0.6775 0.6775 0.677	266.00	5.9927	6.4251	0.7689	0.7696	0.7711	0.7732	0.7761	0.7796	0.7839	0.7888	0.7945
285.00 5.9000 6.3163 0.7458 0.7478 0.7478 0.7394 0.7558 0.7598 0.7694 0.7469 335.00 5.7616 6.1545 0.7121 0.7126 0.7138 0.7137 0.7130 0.7337 0.7247 0.7289 0.7337 334.24 5.7372 6.1262 0.7062 0.7063 0.7080 0.7112 0.7113 0.7120 0.7123 0.7124 0.7289 0.7274 337.10 5.7372 6.1260 0.7065 0.7090 0.7121 0.7113 0.7166 0.7290 0.7124 0.7130 0.7169 355.00 5.6990 6.0171 0.6990 0.6995 0.6986 0.7064 0.7090 0.7130 0.7164 355.00 5.6029 5.9733 0.6744 0.6730 0.6776 0.6783 0.6893 0.6934 0.6736 0.6783 0.6831 0.6868 0.6934 416.00 5.5453 0.6653 0.6652 0.6752 0.6775 0.6751 0.6776	275.36	5.9442	6.3681	0.7568	0.7575	0.7589	0.7609	0.7637	0.7671	0.7712	0.7760	0.7815
308.00 5.8130 6.2145 0.7245 0.7251 0.7282 0.7379 0.7339 0.7376 0.7420 0.7469 332.00 5.7616 6.1545 0.7102 0.7128 0.7181 0.7121 0.7214 0.7228 0.7224 337.10 5.7302 6.1180 0.7062 0.7007 0.7025 0.7044 0.7134 0.7169 0.7212 0.7152 0.7164 0.7135 0.7169 0.7122 0.7152 0.7140 0.7135 0.7169 0.7122 0.7156 0.7009 0.7131 0.7169 0.7112 0.7151 0.7155 0.7055 0.7068 0.7077 0.7035 0.7066 0.7009 0.7130 0.7199 0.7119 0.7114 0.7154 0.555 0.5563 0.6662 0.6681 0.6698 0.6733 0.6749 0.6831 0.8824 0.6826 0.6894 0.68936 0.6799 0.6831 0.6868 0.6694 0.6745 0.6731 0.6767 0.6834 0.6697 0.5544 5.5695 5.5695	285.00	5.9000	6.3163	0.7458	0.7465	0.7478	0.7498	0.7525	0.7558	0.7598	0.7644	0.7697
325.00 5.7616 6.1545 0.7120 0.7126 0.7138 0.7137 0.7211 0.7211 0.7214 0.7214 0.7214 0.7214 0.7214 0.7214 0.7214 0.7214 0.7215 0.7138 0.7215 0.7138 0.7216 0.7226 0.7212 0.7121 0.7130 0.7121 0.7130 0.7121 0.7132 0.7132 0.7121 0.7131 0.7132 0.7121 0.7132 0.7121 0.7132 0.7125 0.7333 355.00 5.6994 6.0810 0.6965 0.6966 0.6706 0.7076 0.7112 0.7112 0.7113 0.7114 0.7114 355.00 5.6960 6.0682 0.6854 0.6863 0.6693 0.6693 0.6693 0.6693 0.6694 0.6794 0.6794 0.6714 0.6724 0.6752 0.6731 0.6799 0.6831 0.6864 0.6793 0.6793 0.6791 0.6733 0.6791 0.6733 0.6791 0.6731 0.6791 0.6731 0.6733 0.6791 0.6731 0.6666 0.6711 0.6711 0.6141 0.6441 0.6464 <	308.00	5.8130	6.2145	0.7245	0.7251	0.7264	0.7282	0.7307	0.7339	0.7376	0.7420	0.7469
332.44 5.7322 6.1262 0.7062 0.7068 0.7097 0.7124 0.7113 0.71169 0.7220 0.7226 337.10 5.7071 6.0911 0.6990 0.6995 0.7007 0.7025 0.7048 0.7077 0.7112 0.7112 0.7112 0.7112 0.7112 0.7113 0.7112 0.7113 0.7112 0.7113 0.7112 0.7113 0.7112 0.7113 0.7090 0.531 0.653 0.6573 0.6773 0.6799 0.6831 0.6834 0.6733 0.6733 0.6745 0.6777 0.613 0.6534 0.6563 0.6563 0.6564 0.6664 0.6773 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6633 0.6544 0.6553 0.6553 0.6553	325.00	5.7616	6.1545	0.7120	0.7126	0.7138	0.7157	0.7181	0.7211	0.7247	0.7289	0.7337
337.10 5.7071 6.011 0.67051 0.7083 0.7080 0.7144 0.7133 0.7169 0.7210 0.7252 351.00 5.6984 6.0810 0.6969 0.6975 0.6986 0.7074 0.7075 0.7056 0.7090 0.7130 0.7179 355.00 5.6906 6.0713 0.6840 0.6826 0.6837 0.6854 0.6676 0.6983 0.6736 0.6936 0.6936 0.6798 0.6821 0.6856 0.6684 0.6679 0.6773 0.6751 0.6773 0.6752 0.6731 0.6763 0.6773 0.6743 0.6774 0.6763 0.6774 0.6743 0.6773 0.6681 0.6669 0.6684 0.6705 0.6731 0.6763 0.6773 0.6813 0.6840 45.799 0.6841 0.6759 0.6841 0.6759 0.6841 0.6759 0.6841 0.6759 0.6841 0.6759 0.6841 0.6759 0.6841 0.6759 0.6651 0.6576 0.6579 0.6611 0.6764 0.6671 0.6741 0.4741 0.4482 0.6484 0.6659 0.6671 0.6741 <	334.24	5.7372	6.1262	0.7062	0.7068	0.7080	0.7097	0.7121	0.7151	0.7186	0.7228	0.7274
347.00 5.7071 6.0911 0.6990 0.6995 0.7007 0.7025 0.7076 0.7112 0.7112 0.7112 351.00 5.6984 6.0810 0.6996 0.6975 0.6986 0.7006 0.7056 0.7090 0.7130 0.7114 0.6741 0.6891 0.6891 0.6891 0.6891 0.6891 0.6891 0.6891 0.6891 0.6891 0.6891 0.6891 0.6813 0.6663 0.6671 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6731 0.6532 <	337.10	5.7302	6.1180	0.7045	0.7051	0.7063	0.7080	0.7104	0.7133	0.7169	0.7210	0.7256
351.00 5.6984 6.0811 0.69649 0.6975 0.6986 0.7027 0.7056 0.7069 0.7130 0.7176 355.00 5.6905 6.0082 0.6826 0.6837 0.6876 0.6876 0.6903 0.6936 0.6894 0.6936 416.10 5.5025 5.9583 0.6774 0.6776 0.6776 0.6773 0.6799 0.6813 0.6884 0.6910 435.96 5.5699 5.9321 0.6667 0.6672 0.6682 0.6684 0.6713 0.6763 0.6779 0.6743 0.6779 0.6843 457.90 5.5484 5.9072 0.6617 0.6622 0.6632 0.6669 0.6694 0.6725 0.6710 0.6813 457.90 5.5484 5.9072 0.6616 0.6524 0.6548 0.6593 0.6623 0.6664 0.6710 0.6711 0.6813 0.6623 0.6524 0.6541 0.6543 0.6633 0.6633 0.6632 0.6551 0.6518 0.6632 0.6651 0.6526 0.6511 0.6632 0.6652 0.6514 0.6464 0.6464 0.646	347.00	5.7071	6.0911	0.6990	0.6995	0.7007	0.7025	0.7048	0.7077	0.7112	0.7152	0.7198
355.00 5.6690 6.0713 0.66420 0.6955 0.66963 0.6706 0.7035 0.7069 0.7109 0.7114 407.90 5.6626 6.06820 0.6744 0.6760 0.6678 0.6678 0.6868 0.6894 0.6868 0.6894 0.6893 0.6893 0.6798 0.6824 0.6868 0.66910 435.96 5.5699 5.9211 0.6667 0.6672 0.6682 0.6698 0.6719 0.6745 0.6777 0.6813 0.6864 457.90 5.5484 5.9072 0.6617 0.6622 0.6663 0.6614 0.6663 0.6664 0.6663 0.6664 0.6663 0.6664 0.6663 0.6664 0.6663 0.6623 0.6614 0.6565 0.6575 0.555 5.5578 0.6518 0.6523 0.6534 0.6544 0.6569 0.6633 0.6674 0.6524 0.6544 0.6569 0.6633 0.6641 0.6633 0.6634 0.6569 0.6531 0.6564 0.6553 0.6633 0.6544 0.6569 0.6518 0.6533 0.6544 0.6569 0.6518 0.6528 <	351.00	5.6984	6.0810	0.6969	0.6975	0.6986	0.7004	0.7027	0.7056	0.7090	0.7130	0.7176
385.15 5.6356 6.0082 0.6820 0.6874 0.6876 0.6876 0.6903 0.6936 0.6974 0.6714 407.90 5.5025 5.9703 0.6674 0.6775 0.6776 0.6779 0.6831 0.6886 0.6910 435.96 5.5699 5.9231 0.6667 0.6672 0.6682 0.6694 0.6775 0.6731 0.6776 0.6731 0.6763 0.6799 0.6841 457.90 5.5484 5.9072 0.6617 0.6622 0.6632 0.6664 0.6705 0.6731 0.6776 0.6763 0.6691 0.6623 0.6663 0.6601 0.6623 0.6663 0.6607 0.518 0.6553 0.6624 0.6554 0.6553 0.6623 0.6653 0.66633 0.6663 0.6673 0.6623 0.6653 0.6623 0.6653 0.6623 0.6653 0.6623 0.6653 0.6623 0.6653 0.6623 0.6653 0.6623 0.6624 0.6454 0.6569 0.6526 0.6561 0.6580 <t< td=""><td>355.00</td><td>5.6900</td><td>6.0713</td><td>0.6949</td><td>0.6955</td><td>0.6966</td><td>0.6983</td><td>0.7006</td><td>0.7035</td><td>0.7069</td><td>0.7109</td><td>0.7154</td></t<>	355.00	5.6900	6.0713	0.6949	0.6955	0.6966	0.6983	0.7006	0.7035	0.7069	0.7109	0.7154
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	385.15	5.6356	6.0082	0.6820	0.6826	0.6837	0.6854	0.6876	0.6903	0.6936	0.6974	0.7018
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	407.90	5.6029	5.9703	0.6744	0.6749	0.6760	0.6776	0.6798	0.6824	0.6856	0.6894	0.6936
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	416.10	5.5925	5.9583	0.6719	0.6725	0.6735	0.6752	0.6773	0.6799	0.6831	0.6868	0.6910
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	435.96	5.5699	5.9321	0.6667	0.6672	0.6682	0.6698	0.6719	0.6745	0.6777	0.6813	0.6854
$ \begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	441.60	5.5640	5.9253	0.6653	0.6658	0.6669	0.6684	0.6705	0.6731	0.6763	0.6799	0.6840
488.00 5.5237 5.8787 0.6560 0.6565 0.6575 0.6590 0.6611 0.6663 0.66666 0.6701 0.6741 514.50 5.5056 5.8579 0.6614 0.6509 0.6524 0.6544 0.6569 0.6598 0.6633 0.66613 563.20 5.4750 5.8370 0.6477 0.6482 0.6492 0.6506 0.6526 0.6511 0.6580 0.6614 0.6653 563.20 5.4750 5.8370 0.6477 0.6482 0.6441 0.6467 0.6500 0.6528 0.6562 0.6600 611.90 5.4585 5.8039 0.6411 0.6426 0.6440 0.6467 0.6495 0.6528 0.6562 0.6600 611.90 5.4465 5.7956 0.6385 0.6399 0.6413 0.6424 0.6446 0.6445 0.6451 0.6555 670.00 5.4403 5.7853 0.6355 0.6360 0.6369 0.6383 0.6412 0.6442 0.6447 0.6427 0.6507 754.00 5.4033 5.7630 0.6324 0.6324 0.6326 <td>457.90</td> <td>5.5484</td> <td>5.9072</td> <td>0.6617</td> <td>0.6622</td> <td>0.6632</td> <td>0.6648</td> <td>0.6669</td> <td>0.6694</td> <td>0.6725</td> <td>0.6761</td> <td>0.6801</td>	457.90	5.5484	5.9072	0.6617	0.6622	0.6632	0.6648	0.6669	0.6694	0.6725	0.6761	0.6801
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	488.00	5.5237	5.8787	0.6560	0.6565	0.6575	0.6590	0.6611	0.6636	0.6666	0.6701	0.6741
532.00 5.4892 5.8493 0.6494 0.6549 0.6524 0.6544 0.6556 0.6538 0.6633 0.6673 546.23 5.4875 5.8370 0.6447 0.6422 0.6656 0.6551 0.6560 0.6524 0.6561 0.6560 0.6524 0.6653 547.10 5.4656 5.8118 0.6427 0.6422 0.6456 0.6475 0.6500 0.6528 0.6562 0.6660 611.90 5.4585 5.8039 0.6411 0.6416 0.6424 0.6443 0.6467 0.6495 0.6528 0.6566 647.10 5.4469 5.7903 0.6385 0.6389 0.6399 0.6413 0.6422 0.64464 0.64466 0.6485 0.6512 0.6562 0.6539 644.30 5.4403 5.7753 0.6355 0.6360 0.6384 0.6383 0.6402 0.6446 0.6447 0.6446 0.6447 0.6524 0.6562 0.6572 0.6534 725.00 5.4268 5.7671 0.6335 0.6344 0.6354 0.6372 0.6383 0.6417 0.6473 0.6473<	514.50	5.5056	5.8579	0.6518	0.6523	0.6533	0.6548	0.6568	0.6593	0.6623	0.6658	0.6697
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	532.00	5.4952	5.8459	0.6494	0.6499	0.6509	0.6524	0.6544	0.6569	0.6598	0.6633	0.6671
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	546.23	5.4875	5.8370	0.6477	0.6482	0.6492	0.6506	0.6526	0.6551	0.6580	0.6614	0.6653
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	504.10	5.4790	0.8273	0.6458	0.6462	0.6472	0.6487	0.6507	0.6531	0.6560	0.6594	0.6632
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	094.10 611.00	5.4030	5.0110	0.0427	0.0432	0.6441	0.0430	0.0475	0.0300	0.0528	0.0502	0.0000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	632.80	5 4515	5.7056	0.6305	0.6410	0.0420	0.6424	0.6443	0.0484 0.6467	0.6312	0.6528	0.0585
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	647.10	5.4313	5.7900	0.6395	0.6280	0.0409	0.6412	0.6422	0.6456	0.6485	0.6517	0.6555
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	670.00	5.4403	5 7826	0.6360	0.6374	0.6384	0.6308	0.6417	0.6441	0.6460	0.6502	0.6530
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	694 30	5 / 339	5 7753	0.6355	0.6360	0.6369	0.0398	0.6402	0.6426	0.6454	0.0302 0.6487	0.0539 0.6524
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	725.00	5 4268	5 7671	0.6339	0.6344	0.6353	0.6367	0.6386	0.6409	0.6437	0.6470	0.6507
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	754.00	5 4208	5 7603	0.6325	0.6330	0.6340	0.6354	0.6372	0.6396	0.6423	0.6456	0.6492
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	785.00	5 4152	5 7539	0.6313	0.6317	0.6327	0.6341	0.6359	0.6383	0.6410	0.6442	0.6479
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	800.00	5.4127	5.7510	0.6307	0.6312	0.6321	0.6335	0.6354	0.6377	0.6405	0.6437	0.6473
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	836.00	5.4073	5.7448	0.6295	0.6300	0.6309	0.6323	0.6341	0.6364	0.6392	0.6424	0.6460
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	876.00	5.4021	5.7388	0.6283	0.6288	0.6297	0.6311	0.6329	0.6352	0.6380	0.6412	0.6448
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	904.00	5.3989	5.7351	0.6276	0.6281	0.6290	0.6304	0.6322	0.6345	0.6372	0.6404	0.6440
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	911.28	5.3981	5.7342	0.6274	0.6279	0.6288	0.6302	0.6320	0.6343	0.6370	0.6402	0.6438
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	946.00	5.3945	5.7301	0.6266	0.6271	0.6280	0.6294	0.6312	0.6335	0.6362	0.6394	0.6430
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	975.00	5.3918	5.7270	0.6260	0.6265	0.6274	0.6288	0.6306	0.6329	0.6356	0.6387	0.6423
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1000.00	5.3897	5.7246	0.6255	0.6260	0.6269	0.6283	0.6301	0.6324	0.6351	0.6383	0.6418
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1064.00	5.3850	5.7192	0.6245	0.6249	0.6259	0.6272	0.6290	0.6313	0.6340	0.6371	0.6407
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1106.00	5.3823	5.7161	0.6239	0.6243	0.6253	0.6266	0.6284	0.6307	0.6334	0.6365	0.6401
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1152.00	5.3797	5.7131	0.6233	0.6238	0.6247	0.6260	0.6278	0.6301	0.6328	0.6359	0.6394
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1185.00	5.3780	5.7112	0.6229	0.6234	0.6243	0.6257	0.6275	0.6297	0.6324	0.6355	0.6391
$ \begin{array}{ccccccccccccccccccccccccc$	1225.00	5.3762	5.7091	0.6225	0.6230	0.6239	0.6252	0.6270	0.6293	0.6320	0.6351	0.6386
$ \begin{array}{ccccccccccccccccccccccccc$	1275.00	5.3741	5.7067	0.6220	0.6225	0.6234	0.6248	0.6266	0.6288	0.6315	0.6346	0.6381
Static 5.3493 5.6783 0.6165 0.6170 0.6179 0.6192 0.6210 0.6232 0.6258 0.6288 0.6323	1320.00	5.3724	5.7048	0.6217	0.6221	0.6230	0.6244	0.6262	0.6284	0.6311	0.6342	0.6377
	Static	5.3493	5.6783	0.6165	0.6170	0.6179	0.6192	0.6210	0.6232	0.6258	0.6288	0.6323

TABLE T6. Mean polarizability matrix elements $\langle \bar{\alpha} \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \bar{\alpha} | \psi_{v',J'} \rangle$ of D₂ for v=1 and v=2.

			ě			,0 0				
$\lambda(\text{nm})$	$\langle \bar{\alpha} \rangle_{20,20}$	$\langle \bar{\alpha} \rangle_{20,10}$	$\langle \bar{\alpha} \rangle_{21,11}$	$\langle \bar{\alpha} \rangle_{22,12}$	$\langle \bar{\alpha} \rangle_{23,13}$	$\langle \bar{\alpha} \rangle_{24,14}$	$\langle \bar{\alpha} \rangle_{25,15}$	$\langle \bar{\alpha} \rangle_{26,16}$	$\langle \bar{\alpha} \rangle_{27,17}$	$\langle \bar{\alpha} \rangle_{28,18}$
182.26	8.3031	1.5610	1.5629	1.5669	1.5729	1.5809	1.5909	1.6030	1.6170	1.6332
193.00	7.9573	1.4503	1.4520	1.4554	1.4606	1.4675	1.4761	1.4864	1.4985	1.5124
213.00	7.5054	1.3103	1.3117	1.3145	1.3187	1.3243	1.3312	1.3396	1.3494	1.3605
222.00	7.3554	1.2650	1.2663	1.2689	1.2728	1.2780	1.2845	1.2923	1.3013	1.3117
224.30	7.3209	1.2547	1.2560	1.2586	1.2624	1.2675	1.2739	1.2815	1.2904	1.3006
235.00	7.1781	1.2124	1.2135	1.2159	1.2195	1.2242	1.2302	1.2373	1.2455	1.2550
248.00	7.0356	1.1707	1.1718	1.1740	1.1773	1.1817	1.1872	1.1938	1.2015	1.2102
266.00	6.8797	1.1257	1.1268	1.1288	1.1318	1.1359	1.1410	1.1470	1.1541	1.1621
275.36	6.8130	1.1067	1.1077	1.1097	1.1126	1.1165	1.1214	1.1272	1.1340	1.1417
285.00	6.7525	1.0896	1.0905	1.0924	1.0953	1.0990	1.1038	1.1094	1.1159	1.1234
308.00	6.6340	1.0563	1.0572	1.0590	1.0616	1.0652	1.0696	1.0749	1.0810	1.0879
325.00	6.5644	1.0370	1.0379	1.0396	1.0421	1.0455	1.0497	1.0548	1.0607	1.0673
334.24	6.5316	1.0279	1.0288	1.0304	1.0329	1.0363	1.0404	1.0454	1.0511	1.0577
337.10	6.5220	1.0253	1.0261	1.0278	1.0303	1.0336	1.0377	1.0427	1.0484	1.0549
347.00	6.4910	1.0168	1.0176	1.0192	1.0217	1.0249	1.0290	1.0338	1.0394	1.0458
351.00	6.4793	1.0136	1.0144	1.0160	1.0184	1.0216	1.0257	1.0305	1.0361	1.0424
355.00	6.4680	1.0105	1.0113	1.0129	1.0153	1.0185	1.0225	1.0273	1.0328	1.0391
385.15	6.3952	0.9906	0.9914	0.9929	0.9952	0.9983	1.0021	1.0067	1.0120	1.0180
407.90	6.3515	0.9788	0.9795	0.9810	0.9833	0.9863	0.9900	0.9944	0.9996	1.0054
416.10	6.3377	0.9750	0.9758	0.9773	0.9795	0.9825	0.9861	0.9906	0.9957	1.0015
435.96	6.3075	0.9669	0.9676	0.9691	0.9713	0.9742	0.9778	0.9821	0.9872	0.9928
441.60	6.2997	0.9648	0.9656	0.9670	0.9692	0.9721	0.9757	0.9800	0.9850	0.9906
457.90	6.2790	0.9592	0.9600	0.9614	0.9636	0.9664	0.9700	0.9742	0.9791	0.9847
488.00	6.2463	0.9505	0.9512	0.9526	0.9547	0.9575	0.9610	0.9652	0.9700	0.9754
514.50	6.2223	0.9441	0.9448	0.9462	0.9483	0.9510	0.9545	0.9586	0.9633	0.9687
532.00	6.2086	0.9405	0.9411	0.9425	0.9446	0.9473	0.9507	0.9548	0.9595	0.9648
546.23	6.1984	0.9377	0.9384	0.9398	0.9418	0.9446	0.9479	0.9520	0.9566	0.9619
563.20	6.1872	0.9348	0.9355	0.9368	0.9389	0.9416	0.9449	0.9489	0.9535	0.9588
594.10	6.1695	0.9301	0.9308	0.9321	0.9341	0.9368	0.9401	0.9440	0.9486	0.9538
611.90	6.1605	0.9277	0.9284	0.9297	0.9317	0.9344	0.9377	0.9416	0.9461	0.9513
632.80	6.1509	0.9252	0.9259	0.9272	0.9292	0.9318	0.9351	0.9390	0.9435	0.9486
647.10	6.1449	0.9236	0.9243	0.9256	0.9276	0.9302	0.9334	0.9373	0.9418	0.9470
670.00	6.1361	0.9213	0.9219	0.9233	0.9252	0.9278	0.9311	0.9349	0.9394	0.9445
694.30	6.1278	0.9191	0.9197	0.9210	0.9230	0.9256	0.9288	0.9327	0.9371	0.9422
725.00	6.1184	0.9166	0.9173	0.9186	0.9205	0.9231	0.9263	0.9301	0.9345	0.9396
754.00	6.1106	0.9146	0.9152	0.9165	0.9184	0.9210	0.9242	0.9280	0.9324	0.9374
785.00	6.1033	0.9126	0.9133	0.9146	0.9165	0.9190	0.9222	0.9260	0.9304	0.9354
800.00	6.1000	0.9118	0.9124	0.9137	0.9156	0.9182	0.9213	0.9251	0.9295	0.9345
836.00	6.0929	0.9099	0.9106	0.9118	0.9137	0.9163	0.9194	0.9232	0.9275	0.9325
876.00	6.0860	0.9081	0.9088	0.9100	0.9119	0.9144	0.9176	0.9213	0.9257	0.9306
904.00	6.0818	0.9070	0.9076	0.9089	0.9108	0.9133	0.9164	0.9202	0.9245	0.9294
911.28	6.0807	0.9067	0.9074	0.9086	0.9105	0.9130	0.9162	0.9199	0.9242	0.9291
946.00	6.0761	0.9055	0.9061	0.9074	0.9093	0.9118	0.9149	0.9186	0.9229	0.9278
975.00	6.0726	0.9046	0.9052	0.9065	0.9084	0.9109	0.9140	0.9177	0.9220	0.9269
1000.00	6.0698	0.9039	0.9045	0.9058	0.9076	0.9101	0.9132	0.9169	0.9212	0.9261
1064.00	6.0636	0.9022	0.9029	0.9041	0.9060	0.9085	0.9116	0.9153	0.9195	0.9244
1106.00	6.0601	0.9013	0.9020	0.9032	0.9051	0.9076	0.9106	0.9143	0.9186	0.9234
1152.00	6.0567	0.9004	0.9011	0.9023	0.9042	0.9066	0.9097	0.9134	0.9176	0.9225
1185.00	6.0545	0.8999	0.9005	0.9017	0.9036	0.9061	0.9091	0.9128	0.9170	0.9219
1225.00	6.0521	0.8992	0.8999	0.9011	0.9030	0.9054	0.9085	0.9121	0.9164	0.9212
1275.00	6.0494	0.8985	0.8991	0.9004	0.9022	0.9047	0.9078	0.9114	0.9156	0.9204
1320.00	6.0472	0.8980	0.8986	0.8998	0.9017	0.9041	0.9072	0.9108	0.9151	0.9198
Static	6.0170	0.8901	0.8907	0.8919	0.8937	0.8961	0.8991	0.9027	0.9068	0.9115

S2. Matrix elements of polarizability anisotropy

$\lambda(\text{nm})$	$\langle \gamma angle_{00,00}$	$\langle \gamma \rangle_{00,02}$	$\langle \gamma \rangle_{01,03}$	$\langle \gamma \rangle_{02,04}$	$\langle \gamma angle_{03,05}$	$\langle \gamma \rangle_{04,06}$	$\langle \gamma \rangle_{05,07}$	$\langle \gamma angle_{06,08}$	$\langle \gamma angle_{07,09}$	$\langle \gamma angle_{08,0\ 10}$
182.26	3.1512	3.1733	3.2026	3.2469	3.3063	3.3813	3.4724	3.5802	3.7055	3.8491
193.00	2.9784	2.9986	3.0255	3.0660	3.1204	3.1889	3.2721	3.3703	3.4843	3.6147
213.00	2.7537	2.7717	2.7955	2.8314	2.8794	2.9400	3.0133	3.0998	3.1998	3.3139
222.00	2.6795	2.6968	2.7196	2.7540	2.8001	2.8581	2.9282	3.0110	3.1066	3.2156
224.30	2.6626	2.6796	2.7023	2.7363	2.7819	2.8393	2.9088	2.9907	3.0853	3.1931
235.00	2.5922	2.6086	2.6303	2.6630	2.7067	2.7618	2.8283	2.9067	2.9973	3.1004
248.00	2.5223	2.5380	2.5588	2.5901	2.6321	2.6848	2.7485	2.8235	2.9101	3.0086
266.00	2.4461	2.4611	2.4809	2.5108	2.5508	2.6011	2.6618	2.7332	2.8155	2.9091
275.36	2.4136	2.4283	2.4477	2.4770	2.5162	2.5654	2.6248	2.6947	2.7753	2.8668
285.00	2.3841	2.3986	2.4176	2.4464	2.4848	2.5331	2.5914	2.6599	2.7389	2.8286
308.00	2.3266	2.3405	2.3589	2.3866	2.4236	2.4701	2.5262	2.5921	2.6680	2.7541
325.00	2.2930	2.3066	2.3246	2.3516	2.3878	2.4333	2.4881	2.5525	2.6266	2.7107
334.24	2.2771	2.2906	2.3084	2.3352	2.3710	2.4159	2.4702	2.5338	2.6071	2.6903
337.10	2.2725	2.2860	2.3037	2.3304	2.3661	2.4109	2.4650	2.5284	2.6015	2.6843
347.00	2.2576	2.2709	2.2884	2.3149	2.3502	2.3945	2.4480	2.5108	2.5831	2.6651
351.00	2.2519	2.2652	2.2827	2.3090	2.3442	2.3884	2.4417	2.5042	2.5762	2.6578
355.00	2.2465	2.2597	2.2771	2.3034	2.3384	2.3825	2.4355	2.4978	2.5696	2.6509
385.15	2.2115	2.2244	2.2414	2.2670	2.3012	2.3442	2.3960	2.4568	2.5267	2.6059
407.90	2.1905	2.2032	2.2200	2.2453	2.2790	2.3213	2.3723	2.4322	2.5010	2.5790
416.10	2.1839	2.1965	2.2133	2.2384	2.2719	2.3141	2.3648	2.4244	2.4929	2.5705
435.96	2.1694	2.1820	2.1985	2.2234	2.2566	2.2983	2.3486	2.4075	2.4753	2.5520
441.60	2.1657	2.1782	2.1947	2.2195	2.2527	2.2942	2.3444	2.4031	2.4707	2.5473
457.90	2.1558	2.1682	2.1846	2.2092	2.2421	2.2834	2.3332	2.3915	2.4586	2.5346
488.00	2.1402	2.1524	2.1686	2.1930	2.2255	2.2664	2.3156	2.3732	2.4395	2.5146
514.50	2.1288	2.1409	2.1570	2.1812	2.2134	2.2539	2.3027	2.3599	2.4256	2.5001
532.00	2.1222	2.1343	2.1503	2.1743	2.2065	2.2468	2.2953	2.3522	2.4176	2.4917
546.23	2.1173	2.1294	2.1453	2.1693	2.2013	2.2415	2.2898	2.3465	2.4117	2.4855
563.20	2.1120	2.1241	2.1399	2.1638	2.1957	2.2357	2.2839	2.3404	2.4053	2.4787
594.10	2.1036	2.1155	2.1313	2.1550	2.1867	2.2265	2.2744	2.3305	2.3950	2.4680
611.90	2.0993	2.1112	2.1270	2.1506	2.1822	2.2218	2.2696	2.3255	2.3898	2.4625
632.80	2.0947	2.1066	2.1223	2.1459	2.1774	2.2169	2.2644	2.3202	2.3842	2.4567
647.10	2.0919	2.1038	2.1194	2.1429	2.1744	2.2138	2.2612	2.3169	2.3808	2.4531
670.00	2.0877	2.0995	2.1151	2.1386	2.1699	2.2092	2.2565	2.3120	2.3757	2.4478
694.30	2.0837	2.0955	2.1111	2.1345	2.1657	2.2049	2.2521	2.3073	2.3708	2.4427
725.00	2.0793	2.0910	2.1065	2.1298	2.1610	2.2000	2.2471	2.3022	2.3654	2.4371
754.00	2.0756	2.0873	2.1028	2.1260	2.1571	2.1960	2.2429	2.2978	2.3609	2.4324
785.00	2.0721	2.0838	2.0992	2.1224	2.1534	2.1922	2.2390	2.2938	2.3567	2.4279
800.00	2.0705	2.0822	2.0976	2.1208	2.1517	2.1905	2.2372	2.2920	2.3548	2.4259
836.00	2.0672	2.0788	2.0942	2.1173	2.1482	2.1868	2.2334	2.2880	2.3507	2.4217
876.00	2.0639	2.0755	2.0909	2.1139	2.1447	2.1833	2.2298	2.2842	2.3468	2.4175
904.00	2.0619	2.0735	2.0888	2.1118	2.1426	2.1811	2.2275	2.2819	2.3443	2.4150
911.28	2.0614	2.0730	2.0883	2.1113	2.1420	2.1806	2.2269	2.2813	2.3437	2.4143
946.00	2.0592	2.0708	2.0861	2.1090	2.1397	2.1782	2.2245	2.2787	2.3410	2.4115
975.00	2.0575	2.0691	2.0844	2.1073	2.1379	2.1764	2.2226	2.2768	2.3390	2.4094
1000.00	2.0562	2.0678	2.0830	2.1059	2.1366	2.1749	2.2211	2.2753	2.3374	2.4078
1064.00	2.0533	2.0648	2.0800	2.1029	2.1334	2.1717	2.2178	2.2718	2.3339	2.4040
1106.00	2.0516	2.0631	2.0783	2.1012	2.1317	2.1699	2.2160	2.2699	2.3318	2.4019
1152.00	2.0500	2.0615	2.0767	2.0995	2.1300	2.1682	2.2141	2.2680	2.3299	2.3999
1185.00	2.0490	2.0605	2.0756	2.0984	2.1289	2.1670	2.2130	2.2668	2.3286	2.3985
1225.00	2.0478	2.0593	2.0745	2.0972	2.1276	2.1658	2.2117	2.2655	2.3272	2.3971
1275.00	2.0465	2.0580	2.0731	2.0959	2.1263	2.1644	2.2102	2.2640	2.3257	2.3954
1320.00	2.0455	2.0570	2.0721	2.0948	2.1252	2.1633	2.2091	2.2628	2.3244	2.3941
Static	2.0312	2.0426	2.0575	2.0800	2.1101	2.1477	2.1930	2.2461	2.3071	2.3760

TABLE T7. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of H₂ for v=0.

TABLE T8. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of H₂ for v=1.

$\lambda(\text{nm})$	$\langle \gamma angle_{10,10}$	$\langle \gamma angle_{10,12}$	$\langle \gamma \rangle_{11,13}$	$\langle \gamma angle_{12,14}$	$\langle \gamma angle_{13,15}$	$\langle \gamma \rangle_{14,16}$	$\langle \gamma angle_{15,17}$	$\langle \gamma angle_{16,18}$	$\langle \gamma angle_{17,19}$	$\langle \gamma angle_{18,110}$
182.26	4.2412	4.2695	4.3064	4.3621	4.4370	4.5316	4.6468	4.7832	4.9421	5.1245
193.00	3.9516	3.9769	4.0097	4.0593	4.1260	4.2100	4.3121	4.4329	4.5731	4.7338
213.00	3.5868	3.6084	3.6365	3.6788	3.7356	3.8072	3.8939	3.9963	4.1147	4.2499
222.00	3.4690	3.4895	3.5162	3.5563	3.6101	3.6778	3.7598	3.8565	3.9683	4.0958
224.30	3.4423	3.4625	3.4888	3.5284	3.5816	3.6484	3.7294	3.8248	3.9351	4.0609
235.00	3.3321	3.3514	3.3763	3.4139	3.4643	3.5276	3.6043	3.6946	3.7989	3.9177
248.00	3.2238	3.2421	3.2657	3.3014	3.3491	3.4091	3.4817	3.5671	3.6657	3.7778
266.00	3.1071	3.1243	3.1466	3.1802	3.2252	3.2817	3.3499	3.4302	3.5227	3.6279
275.36	3.0577	3.0745	3.0963	3.1290	3.1728	3.2278	3.2943	3.3724	3.4625	3.5648
285.00	3.0132	3.0296	3.0508	3.0828	3.1255	3.1793	3.2442	3.3204	3.4082	3.5079
308.00	2.9268	2.9425	2.9628	2.9933	3.0341	3.0853	3.1471	3.2197	3.3033	3.3982
325.00	2.8766	2.8919	2.9116	2.9412	2.9809	3.0307	3.0908	3.1614	3.2425	3.3346
334.24	2.8530	2.8681	2.8876	2.9168	2.9560	3.0051	3.0644	3.1340	3.2140	3.3048
337.10	2.8462	2.8612	2.8806	2.9098	2.9488	2.9977	3.0568	3.1260	3.2058	3.2961
347.00	2.8240	2.8389	2.8580	2.8868	2.9253	2.9736	3.0319	3.1003	3.1790	3.2682
351.00	2.8157	2.8304	2.8495	2.8782	2.9165	2.9646	3.0226	3.0906	3.1689	3.2576
355.00	2.8077	2.8224	2.8413	2.8699	2.9080	2.9559	3.0136	3.0813	3.1593	3.2475
385.15	2.7560	2.7703	2.7887	2.8164	2.8534	2.8999	2.9559	3.0216	3.0971	3.1826
407.90	2.7253	2.7393	2.7574	2.7846	2.8209	2.8666	2.9215	2.9860	3.0601	3.1439
416.10	2.7156	2.7295	2.7475	2.7745	2.8107	2.8560	2.9107	2.9747	3.0484	3.1317
435.96	2.6944	2.7082	2.7260	2.7527	2.7884	2.8331	2.8871	2.9503	3.0230	3.1052
441.60	2.6890	2.7027	2.7204	2.7470	2.7826	2.8272	2.8810	2.9441	3.0165	3.0984
457.90	2.6745	2.6881	2.7057	2.7320	2.7673	2.8115	2.8648	2.9273	2.9991	3.0803
488.00	2.6517	2.6652	2.6825	2.7085	2.7433	2.7869	2.8395	2.9011	2.9718	3.0518
514.50	2.6351	2.6484	2.6656	2.6913	2.7258	2.7690	2.8210	2.8819	2.9519	3.0311
532.00	2.6256	2.6388	2.6559	2.6815	2.7157	2.7586	2.8104	2.8709	2.9405	3.0192
546.23	2.6185	2.6317	2.6487	2.6742	2.7083	2.7510	2.8025	2.8628	2.9321	3.0104
563.20	2.6109	2.6240	2.6409	2.6663	2.7002	2.7427	2.7940	2.8540	2.9229	3.0008
594.10	2.5986	2.6116	2.6284	2.6536	2.6873	2.7295	2.7803	2.8399	2.9082	2.9855
611.90	2.5924	2.6054	2.6221	2.6472	2.6807	2.7228	2.7734	2.8328	2.9009	2.9778
632.80	2.5859	2.5988	2.6154	2.6404	2.6738	2.7157	2.7661	2.8252	2.8930	2.9696
647.10	2.5817	2.5946	2.6112	2.6361	2.6695	2.7112	2.7615	2.8204	2.8881	2.9645
670.00	2.5757	2.5885	2.6051	2.6299	2.6631	2.7047	2.7548	2.8135	2.8809	2.9570
694.30	2.5700	2.5827	2.5992	2.6240	2.6570	2.6985	2.7484	2.8069	2.8740	2.9499
725.00	2.5635	2.5763	2.5927	2.6173	2.6503	2.6916	2.7413	2.7995	2.8663	2.9419
754.00	2.5582	2.5709	2.5873	2.6118	2.6447	2.6858	2.7354	2.7934	2.8600	2.9352
785.00	2.5532	2.5658	2.5821	2.6066	2.6393	2.6804	2.7298	2.7876	2.8540	2.9290
800.00	2.5509	2.3030	2.5799	2.6043	2.0370	2.0780	2.7273	2.7850	2.8513	2.9262
836.00	2.5461	2.5587	2.5749	2.5993	2.0319	2.0727	2.7219	2.7795	2.8455	2.9202
876.00	2.5414	2.5540	2.5702	2.5945	2.0270	2.00//	2.7107	2.7707	2.8399	2.9144
904.00	2.0000	2.5510	2.3072	2.5915	2.0239	2.0040	2.7155	2.7707	2.0300	2.9107
911.20	2.0010	2.0000	2.0000	2.3907	2.0231	2.0030	2.7127	2.7099	2.0000	2.9099
940.00	2.0040	2.5471	2.5052	2.3673	2.0198	2.0003	2.7091	2.7003	2.0010	2.9039
1000.00	2.0022	2.0447	2.5008	2.3830	2.0175	2.0076	2.7005	2.7055	2.8290	2.9030
1064.00	2.5505	2.5428	2.5569	2.3630	2.0155	2.0557	2.7044	2.7014	2.8207	2.9000
1106.00	2.5201	2.0000	2.0040	2.5101	2.0100	2.0312	2.0997	2.1303	2.0417	2.0904
1152.00	2.5257	2.0002	2.0022	2.5702	2.0000	2.0400	2.0970	2.7556	2.0109	2.0924
1185.00	2.5214 2.5100	2.0000 2.5303	2.0490	2.5730	2.0039	2.0401	2.0940	2.7311	2.0101	2.0090
1225.00	2.5183	2.5325	2.5466	2.5725	2.0043	2.6497	2.6920	2.7454	2.8194	2.8856
1225.00	2.5164	2.5588	2.5400	2.5785	2.0020	2.6407	2.6510	2.1410	2.0124	2.8832
1320.00	2.5104 2.5149	2.5268 2.5273	2.5432	2.5671	2.5001	2.6391	2.6873	2.7434	2.8102	2.8815
Static	2.0145	2.5213	2.5224	2.5460	2.5551 2.5775	2.0001 2.6170	2.6645	2 7202	2.0004 2 7840	2.8561
Duatic	2.1010	2.0001	2.0224	2.0400	2.0110	2.0110	2.0040	2.1202	2.1040	2.0001

TABLE T9. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of H₂ for v=2.

$\lambda(\text{nm})$	$\langle \gamma angle_{20,20}$	$\langle \gamma angle_{20,22}$	$\langle \gamma \rangle_{21,23}$	$\langle \gamma \rangle_{22,24}$	$\langle \gamma \rangle_{23,25}$	$\langle \gamma \rangle_{24,26}$	$\langle \gamma \rangle_{25,27}$	$\langle \gamma angle_{26,28}$	$\langle \gamma \rangle_{27,29}$	$\langle \gamma angle_{28,210}$
182.26	5.6158	5.6518	5.6982	5.7683	5.8626	5.9820	6.1275	6.3001	6.5015	6.7332
193.00	5.1504	5.1816	5.2216	5.2820	5.3632	5.4657	5.5903	5.7379	5.9094	6.1061
213.00	4.5828	4.6085	4.6413	4.6907	4.7570	4.8407	4.9420	5.0616	5.2001	5.3582
222.00	4.4040	4.4280	4.4587	4.5048	4.5668	4.6448	4.7392	4.8506	4.9794	5.1263
224.30	4.3636	4.3873	4.4175	4.4629	4.5239	4.6006	4.6936	4.8031	4.9298	5.0743
235.00	4.1986	4.2208	4.2491	4.2916	4.3487	4.4205	4.5073	4.6096	4.7278	4.8623
248.00	4.0381	4.0589	4.0854	4.1252	4.1785	4.2456	4.3267	4.4222	4.5323	4.6576
266.00	3.8670	3.8864	3.9110	3.9480	3.9975	4.0597	4.1349	4.2233	4.3252	4.4409
275.36	3.7952	3.8140	3.8378	3.8736	3.9216	3.9819	4.0546	4.1402	4.2387	4.3504
285.00	3.7307	3.7490	3.7721	3.8069	3.8535	3.9120	3.9826	4.0656	4.1611	4.2695
308.00	3.6065	3.6238	3.6456	3.6785	3.7224	3.7776	3.8442	3.9223	4.0122	4.1141
325.00	3.5348	3.5515	3.5726	3.6044	3.6468	3,7001	3.7644	3.8398	3.9265	4.0248
334.24	3.5012	3.5177	3.5385	3.5697	3.6115	3.6639	3.7271	3.8013	3.8865	3.9831
337.10	3.4915	3.5079	3.5286	3.5597	3.6012	3.6534	3.7163	3.7901	3.8750	3.9710
347.00	3.4601	3.4762	3.4966	3.5272	3.5681	3.6195	3.6814	3.7540	3.8375	3.9320
351.00	3.4482	3.4643	3.4845	3.5150	3.5556	3.6067	3.6683	3.7405	3.8234	3.9173
355.00	3.4369	3.4528	3.4730	3.5032	3.5437	3.5945	3.6557	3.7274	3.8099	3.9032
385.15	3.3640	3.3794	3.3988	3.4280	3.4670	3.5159	3.5749	3.6440	3.7234	3.8131
407.90	3.3207	3.3358	3.3548	3.3833	3.4215	3.4693	3.5270	3.5945	3.6721	3.7598
416.10	3.3070	3.3220	3.3409	3.3692	3.4071	3.4546	3.5118	3.5789	3.6559	3.7430
435.96	3.2774	3.2922	3.3108	3.3387	3.3760	3.4228	3.4791	3.5451	3.6209	3.7065
441.60	3.2698	3.2845	3.3030	3.3308	3.3680	3.4146	3.4707	3.5364	3.6119	3.6972
457.90	3.2496	3.2641	3.2824	3.3099	3.3467	3.3928	3.4483	3.5133	3.5879	3.6723
488.00	3.2178	3.2321	3.2501	3.2772	3.3133	3.3586	3.4132	3.4771	3.5504	3.6333
514.50	3.1947	3.2088	3.2266	3.2533	3.2890	3.3338	3.3877	3.4508	3.5232	3.6049
532.00	3.1814	3.1955	3.2131	3.2396	3.2751	3.3195	3.3730	3.4357	3.5075	3.5887
546.23	3.1716	3.1856	3.2031	3.2295	3.2648	3.3090	3.3622	3.4245	3.4960	3.5767
563.20	3.1609	3.1748	3.1923	3.2185	3.2536	3.2975	3.3504	3.4124	3.4834	3.5636
594.10	3.1439	3.1577	3.1750	3.2010	3.2358	3.2793	3.3317	3.3931	3.4634	3.5428
611.90	3.1354	3.1491	3.1663	3.1922	3.2268	3.2701	3.3222	3.3833	3.4533	3.5324
632.80	3.1262	3.1399	3.1570	3.1828	3.2172	3.2603	3.3122	3.3729	3.4426	3.5212
647.10	3.1205	3.1342	3.1512	3.1769	3.2112	3.2542	3.3059	3.3665	3.4359	3.5142
670.00	3.1122	3.1257	3.1427	3.1683	3.2024	3.2452	3.2967	3.3570	3.4261	3.5040
694.30	3.1042	3.1177	3.1347	3.1601	3.1941	3.2367	3.2879	3.3479	3.4167	3.4943
725.00	3.0953	3.1088	3.1256	3.1510	3.1848	3.2272	3.2782	3.3379	3.4063	3.4835
754.00	3.0880	3.1014	3.1182	3.1434	3.1770	3.2193	3.2701	3.3295	3.3976	3.4745
785.00	3.0810	3.0944	3.1111	3.1362	3.1697	3.2118	3.2624	3.3216	3.3895	3.4660
800.00	3.0779	3.0913	3.1080	3.1330	3.1665	3.2085	3.2590	3.3181	3.3859	3.4623
836.00	3.0712	3.0845	3.1012	3.1261	3.1595	3.2013	3.2516	3.3105	3.3780	3.4541
876.00	3.0648	3.0780	3.0946	3.1195	3.1527	3.1944	3.2445	3.3032	3.3704	3.4463
904.00	3.0608	3.0740	3.0905	3.1153	3.1485	3.1901	3.2401	3.2986	3.3657	3.4414
911.28	3.0598	3.0730	3.0895	3.1143	3.1475	3.1890	3.2390	3.2975	3.3646	3.4402
946.00	3.0554	3.0686	3.0851	3.1098	3.1429	3.1844	3.2342	3.2926	3.3594	3.4349
975.00	3.0521	3.0653	3.0817	3.1064	3.1395	3.1808	3.2306	3.2888	3.3556	3.4309
1000.00	3.0495	3.0627	3.0791	3.1038	3.1367	3.1780	3.2277	3.2859	3.3525	3.4277
1064.00	3.0437	3.0568	3.0732	3.0977	3.1306	3.1718	3.2213	3.2793	3.3457	3.4206
1106.00	3.0404	3.0535	3.0698	3.0944	3.1272	3.1683	3.2177	3.2755	3.3418	3.4166
1152.00	3.0372	3.0503	3.0666	3.0911	3.1238	3.1649	3.2142	3.2719	3.3381	3.4127
1185.00	3.0352	3.0482	3.0645	3.0890	3.1217	3.1626	3.2119	3.2696	3.3357	3.4102
1225.00	3.0329	3.0459	3.0622	3.0866	3.1193	3.1602	3.2094	3.2670	3.3330	3.4075
1275.00	3.0304	3.0433	3.0596	3.0840	3.1166	3.1575	3.2066	3.2642	3.3300	3.4044
1320.00	3.0283	3.0413	3.0575	3.0819	3.1145	3.1553	3.2044	3.2619	3.3277	3.4019
Static	3.0002	3.0130	3.0289	3.0529	3.0850	3.1252	3.1735	3.2300	3.2947	3.3677

TABLE T10. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of HD for v=0.

$\lambda(\text{nm})$	$\langle \gamma angle_{00,00}$	$\langle \gamma angle_{00,02}$	$\langle \gamma \rangle_{01,03}$	$\langle \gamma \rangle_{02,04}$	$\langle \gamma angle_{03,05}$	$\langle \gamma angle_{04,06}$	$\langle \gamma \rangle_{05,07}$	$\langle \gamma angle_{06,08}$	$\langle \gamma angle_{07,09}$	$\langle \gamma angle_{08,010}$
182.26	3.0835	3.0998	3.1215	3.1541	3.1977	3.2528	3.3194	3.3979	3.4888	3.5924
193.00	2.9175	2.9325	2.9523	2.9823	3.0223	3.0727	3.1337	3.2056	3.2885	3.3831
213.00	2.7011	2.7144	2.7321	2.7586	2.7942	2.8389	2.8929	2.9563	3.0296	3.1128
222.00	2.6295	2.6423	2.6593	2.6847	2.7189	2.7617	2.8134	2.8743	2.9444	3.0240
224.30	2.6131	2.6258	2.6426	2.6678	2.7016	2.7440	2.7953	2.8555	2.9249	3.0037
235.00	2.5452	2.5573	2.5734	2.5977	2.6301	2.6708	2.7200	2.7777	2.8443	2.9198
248.00	2.4775	2.4892	2.5047	2.5279	2.5591	2.5981	2.6452	2.7006	2.7643	2.8366
266.00	2.4038	2.4149	2.4297	2.4519	2.4816	2.5189	2.5638	2.6166	2.6773	2.7461
275.36	2.3723	2.3833	2.3977	2.4195	2.4486	2.4851	2.5291	2.5808	2.6402	2.7076
285.00	2.3438	2.3545	2.3687	2.3901	2.4186	2.4545	2.4977	2.5484	2.6067	2.6727
308.00	2.2880	2.2984	2.3121	2.3327	2.3602	2.3948	2.4364	2.4852	2.5413	2.6048
325.00	2.2554	2.2655	2.2789	2.2991	2.3260	2.3598	2.4005	2.4482	2.5030	2.5651
334.24	2.2400	2.2501	2.2633	2.2833	2.3099	2.3433	2.3836	2.4308	2.4850	2.5464
337.10	2.2355	2.2456	2.2588	2.2787	2.3052	2.3386	2.3787	2.4257	2.4798	2.5410
347.00	2.2210	2.2309	2.2440	2.2637	2.2900	2.3230	2.3628	2.4093	2.4628	2.5234
351.00	2.2156	2.2254	2.2385	2.2581	2.2843	2.3172	2.3567	2.4031	2.4564	2.5168
355.00	2.2103	2.2201	2.2331	2.2527	2.2788	2.3115	2.3510	2.3972	2.4503	2.5104
385.15	2.1763	2.1859	2.1986	2.2177	2.2432	2.2752	2.3137	2.3588	2.4106	2.4692
407.90	2.1559	2.1654	2.1779	2.1968	2.2219	2.2534	2.2914	2.3358	2.3868	2.4446
416.10	2.1495	2.1589	2.1714	2.1901	2.2151	2.2465	2.2843	2.3285	2.3793	2.4368
435.96	2.1355	2.1448	2.1571	2.1757	2.2005	2.2315	2.2689	2.3127	2.3630	2.4198
441.60	2.1318	2.1412	2.1535	2.1720	2.1967	2.2277	2.2649	2.3086	2.3588	2.4154
457.90	2.1222	2.1314	2.1437	2.1620	2.1866	2.2173	2.2544	2.2977	2.3475	2.4038
488.00	2.1070	2.1162	2.1283	2.1464	2.1707	2.2011	2.2377	2.2806	2.3298	2.3855
514.50	2.0959	2.1050	2.1170	2.1350	2.1591	2.1893	2.2256	2.2681	2.3169	2.3721
532.00	2.0895	2.0986	2.1105	2.1284	2.1524	2.1824	2.2186	2.2609	2.3095	2.3644
546.23	2.0848	2.0938	2.1057	2.1236	2.1475	2.1774	2.2134	2.2556	2.3040	2.3587
563.20	2.0796	2.0886	2.1005	2.1183	2.1421	2.1719	2.2078	2.2498	2.2980	2.3525
594.10	2.0714	2.0803	2.0921	2.1098	2.1335	2.1631	2.1988	2.2405	2.2885	2.3426
611.90	2.0673	2.0762	2.0879	2.1056	2.1291	2.1587	2.1942	2.2359	2.2836	2.3376
632.80	2.0628	2.0717	2.0834	2.1010	2.1245	2.1540	2.1894	2.2309	2.2785	2.3323
647.10	2.0601	2.0689	2.0806	2.0982	2.1216	2.1510	2.1864	2.2278	2.2753	2.3289
670.00	2.0560	2.0648	2.0765	2.0940	2.1174	2.1467	2.1819	2.2232	2.2705	2.3240
694.30	2.0521	2.0609	2.0726	2.0900	2.1133	2.1425	2.1777	2.2188	2.2660	2.3194
725.00	2.0478	2.0566	2.0682	2.0856	2.1088	2.1379	2.1730	2.2140	2.2610	2.3142
754.00	2.0442	2.0530	2.0645	2.0819	2.1050	2.1341	2.1690	2.2099	2.2568	2.3099
785.00	2.0408	2.0495	2.0611	2.0784	2.1015	2.1305	2.1653	2.2061	2.2529	2.3058
800.00	2.0393	2.0480	2.0595	2.0768	2.0999	2.1289	2.1637	2.2044	2.2512	2.3040
836.00	2.0360	2.0447	2.0562	2.0735	2.0965	2.1254	2.1601	2.2007	2.2473	2.3000
876.00	2.0329	2.0415	2.0530	2.0702	2.0932	2.1220	2.1566	2.1972	2.2437	2.2962
904.00	2.0309	2.0395	2.0510	2.0682	2.0911	2.1199	2.1545	2.1950	2.2414	2.2938
911.28	2.0304	2.0391	2.0505	2.0677	2.0906	2.1194	2.1539	2.1944	2.2408	2.2933
946.00	2.0283	2.0369	2.0483	2.0655	2.0884	2.1171	2.1516	2.1920	2.2383	2.2907
975.00	2.0266	2.0353	2.0467	2.0638	2.0867	2.1154	2.1498	2.1902	2.2365	2.2888
1000.00	2.0254	2.0340	2.0454	2.0625	2.0854	2.1140	2.1484	2.1888	2.2350	2.2872
1064.00	2.0225	2.0311	2.0425	2.0596	2.0824	2.1109	2.1453	2.1855	2.2317	2.2838
1106.00	2.0209	2.0295	2.0408	2.0579	2.0807	2.1092	2.1435	2.1837	2.2298	2.2818
1152.00	2.0193	2.0279	2.0393	2.0563	2.0790	2.1075	2.1418	2.1820	2.2280	2.2800
1185.00	2.0183	2.0269	2.0382	2.0553	2.0780	2.1065	2.1407	2.1808	2.2268	2.2787
1225.00	2.0172	2.0258	2.0371	2.0541	2.0768	2.1053	2.1395	2.1796	2.2255	2.2774
1275.00	2.0159	2.0245	2.0358	2.0528	2.0755	2.1039	2.1381	2.1782	2.2241	2.2759
1320.00	2.0149	2.0235	2.0348	2.0518	2.0745	2.1029	2.1370	2.1770	2.2229	2.2747
Static	2.0010	2.0095	2.0207	2.0375	2.0599	2.0880	2.1219	2.1614	2.2068	2.2580

TABLE T11. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of HD for v=1.

$\lambda(\text{nm})$	$\langle \gamma \rangle_{10,10}$	$\langle \gamma angle_{10,12}$	$\langle \gamma angle_{11,13}$	$\langle \gamma angle_{12,14}$	$\langle \gamma \rangle_{13,15}$	$\langle \gamma angle_{14,16}$	$\langle \gamma \rangle_{15,17}$	$\langle \gamma angle_{16,18}$	$\langle \gamma \rangle_{17,19}$	$\langle \gamma angle_{18,110}$
182.26	3.9975	4.0177	4.0441	4.0839	4.1372	4.2045	4.2860	4.3822	4.4937	4.6210
193.00	3.7362	3.7544	3.7780	3.8137	3.8615	3.9217	3.9945	4.0804	4.1797	4.2929
213.00	3.4048	3.4204	3.4408	3.4715	3.5126	3.5644	3.6269	3.7004	3.7852	3.8817
222.00	3.2973	3.3121	3.3315	3.3607	3.3998	3.4488	3.5081	3.5779	3.6582	3.7496
224.30	3.2728	3.2875	3.3067	3.3355	3.3741	3.4226	3.4811	3.5500	3.6294	3.7196
235.00	3.1719	3.1859	3.2041	3.2316	3.2683	3.3144	3.3700	3.4354	3.5107	3.5963
248.00	3.0725	3.0858	3.1032	3.1292	3.1641	3.2079	3.2607	3.3227	3.3942	3.4752
266.00	2.9651	2.9777	2.9941	3.0187	3.0517	3.0930	3.1429	3.2014	3.2687	3.3450
275.36	2.9196	2.9319	2.9479	2.9719	3.0041	3.0444	3.0930	3.1501	3.2157	3.2900
285.00	2.8785	2.8906	2.9062	2.9297	2.9611	3.0005	3.0480	3.1037	3.1678	3.2404
308.00	2.7987	2.8103	2.8252	2.8477	2.8777	2.9154	2.9608	3.0140	3.0752	3.1444
325.00	2.7523	2.7635	2.7781	2.8000	2.8292	2.8659	2.9101	2.9618	3.0214	3.0887
334.24	2.7305	2.7416	2.7559	2.7775	2.8064	2.8426	2.8862	2.9374	2.9961	3.0626
337.10	2.7242	2.7352	2.7495	2.7710	2.7998	2.8359	2.8793	2.9303	2.9888	3.0550
347.00	2.7036	2.7145	2.7287	2.7499	2.7784	2.8140	2.8569	2.9072	2.9650	3.0304
351.00	2.6959	2.7067	2.7208	2.7420	2.7703	2.8058	2.8485	2.8986	2.9561	3.0211
355.00	2.6884	2.6993	2.7133	2.7344	2.7625	2.7979	2.8404	2.8902	2.9475	3.0122
385.15	2.6406	2.6511	2.6647	2.6852	2.7126	2.7469	2.7882	2.8366	2.8922	2.9550
407.90	2.6120	2.6224	2.6358	2.6559	2.6828	2.7165	2.7571	2.8047	2.8593	2.9210
416.10	2.6030	2.6133	2.6266	2.6466	2.6734	2.7069	2.7473	2.7946	2.8489	2.9102
435.96	2.5834	2.5935	2.6067	2.6265	2.6529	2.6861	2.7259	2.7726	2.8262	2.8868
441.60	2.5783	2.5884	2.6016	2.6213	2.6477	2.6807	2.7204	2.7670	2.8204	2.8808
457.90	2.5648	2.5749	2.5879	2.6075	2.6336	2.6664	2.7058	2.7520	2.8049	2.8648
488.00	2.5437	2.5536	2.5664	2.5858	2.6116	2.6439	2.6828	2.7283	2.7806	2.8396
514.50	2.5282	2.5381	2.5508	2.5699	2.5955	2.6275	2.6660	2.7111	2.7628	2.8213
532.00	2.5194	2.5291	2.5418	2.5608	2.5862	2.6181	2.6564	2.7012	2.7526	2.8107
546.23	2.5128	2.5225	2.5351	2.5541	2.5794	2.6111	2.6492	2.6939	2.7451	2.8030
563.20	2.5057	2.5153	2.5279	2.5468	2.5719	2.6035	2.6415	2.6859	2.7369	2.7945
594.10	2.4943	2.5039	2.5163	2.5351	2.5601	2.5914	2.6291	2.6732	2.7238	2.7810
611.90	2.4885	2.4981	2.5105	2.5292	2.5541	2.5853	2.6228	2.6668	2.7172	2.7741
632.80	2.4824	2.4919	2.5043	2.5229	2.5477	2.5788	2.6162	2.6600	2.7102	2.7669
647.10	2.4785	2.4881	2.5004	2.5189	2.5437	2.5747	2.6120	2.6557	2.7058	2.7623
670.00	2.4729	2.4824	2.4947	2.5132	2.5378	2.5687	2.6059	2.6494	2.6993	2.7556
694.30	2.4676	2.4770	2.4893	2.5077	2.5323	2.5631	2.6001	2.6435	2.6932	2.7493
725.00	2.4616	2.4710	2.4832	2.5016	2.5260	2.5567	2.5936	2.6368	2.6863	2.7422
754.00	2.4566	2.4660	2.4782	2.4965	2.5209	2.5514	2.5882	2.6313	2.6806	2.7363
785.00	2.4519	2.4613	2.4734	2.4916	2.5160	2.5465	2.5831	2.6260	2.6752	2.7308
800.00	2.4498	2.4592	2.4713	2.4895	2.5138	2.5443	2.5809	2.6237	2.6729	2.7283
836.00	2.4453	2.4547	2.4667	2.4849	2.5091	2.5395	2.5760	2.6187	2.6677	2.7230
876.00	2.4410	2.4503	2.4623	2.4804	2.5046	2.5348	2.5712	2.6138	2.6627	2.7178
904.00	2.4382	2.4475	2.4596	2.4776	2.5017	2.5320	2.5683	2.6108	2.6596	2.7146
911.28	2.4376	2.4469	2.4589	2.4769	2.5011	2.5312	2.5676	2.6101	2.6588	2.7138
946.00	2.4346	2.4439	2.4559	2.4739	2.4980	2.5281	2.5644	2.6068	2.6554	2.7103
975.00	2.4324	2.4417	2.4536	2.4716	2.4957	2.5258	2.5620	2.6043	2.6529	2.7077
1000.00	2.4306	2.4399	2.4519	2.4698	2.4938	2.5239	2.5600	2.6023	2.6508	2.7056
1064.00	2.4267	2.4359	2.4479	2.4658	2.4897	2.5197	2.5558	2.5980	2.6463	2.7009
1106.00	2.4245	2.4337	2.4456	2.4635	2.4874	2.5173	2.5534	2.5955	2.6438	2.6983
1152.00	2.4223	2.4315	2.4434	2.4613	2.4852	2.5151	2.5510	2.5931	2.6413	2.6958
1185.00	2.4209	2.4301	2.4420	2.4599	2.4837	2.5136	2.5495	2.5915	2.6397	2.6941
1225.00	2.4194	2.4286	2.4404	2.4583	2.4821	2.5119	2.5478	2.5898	2.6380	2.6923
1275.00	2.4177	2.4268	2.4387	2.4565	2.4803	2.5101	2.5460	2.5879	2.6360	2.6902
1320.00	2.4163	2.4254	2.4373	2.4551	2.4789	2.5087	2.5445	2.5864	2.6344	2.6886
Static	2.3972	2.4062	2.4179	2.4355	2.4590	2.4884	2.5238	2.5651	2.6125	2.6660

TABLE T12. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of HD for v=2.

						'		,		
$\lambda(\text{nm})$	$\langle \gamma angle_{20,20}$	$\langle \gamma angle_{20,22}$	$\langle \gamma \rangle_{21,23}$	$\langle \gamma \rangle_{22,24}$	$\langle \gamma \rangle_{23,25}$	$\langle \gamma \rangle_{24,26}$	$\langle \gamma \rangle_{25,27}$	$\langle \gamma \rangle_{26,28}$	$\langle \gamma \rangle_{27,29}$	$\langle \gamma \rangle_{28,210}$
182.26	5.1149	5.1398	5.1720	5.2205	5.2857	5.3679	5.4676	5.5854	5.7220	5.8783
193.00	4.7176	4.7394	4.7675	4.8099	4.8667	4.9382	5.0249	5.1271	5.2454	5.3803
213.00	4.2274	4.2456	4.2690	4.3042	4.3514	4.4107	4.4824	4.5668	4.6643	4.7752
222.00	4.0716	4.0887	4.1107	4.1437	4.1880	4.2437	4.3109	4.3900	4.4813	4.5850
224.30	4.0363	4.0532	4.0749	4.1074	4.1511	4.2059	4.2722	4.3501	4.4400	4.5421
235.00	3.8918	3.9078	3.9281	3.9588	3.9998	4.0514	4.1137	4.1868	4.2711	4.3669
248.00	3.7508	3.7658	3.7850	3.8138	3.8524	3.9008	3.9593	4.0279	4.1070	4.1966
266.00	3.5999	3.6139	3.6318	3.6587	3.6947	3.7399	3.7944	3.8584	3.9320	4.0154
275.36	3.5364	3.5500	3.5674	3.5935	3.6284	3.6723	3.7252	3.7872	3.8586	3.9394
285.00	3.4792	3.4925	3.5094	3.5348	3.5688	3.6115	3.6630	3.7233	3.7927	3.8712
308.00	3.3689	3.3815	3.3976	3.4217	3.4539	3.4943	3.5430	3.6001	3.6657	3.7400
325.00	3.3051	3.3173	3.3328	3.3562	3.3874	3.4265	3.4737	3.5289	3.5924	3.6642
334.24	3.2752	3.2872	3.3025	3.3255	3.3563	3.3948	3.4412	3.4956	3.5581	3.6288
337.10	3.2665	3.2785	3.2937	3.3166	3.3472	3.3856	3.4318	3.4860	3.5482	3.6185
347.00	3.2384	3.2503	3.2653	3.2879	3.3180	3.3558	3.4014	3.4547	3.5160	3.5853
351.00	3.2279	3.2396	3.2546	3.2770	3.3070	3.3446	3.3899	3.4430	3.5039	3.5728
355.00	3.2177	3.2294	3.2443	3.2666	3.2965	3.3339	3.3789	3.4317	3.4923	3.5608
385.15	3.1526	3.1639	3.1783	3.1999	3.2287	3.2649	3.3084	3.3593	3.4178	3.4840
407.90	3.1139	3.1250	3.1390	3.1602	3.1884	3.2238	3.2665	3.3164	3.3736	3.4383
416.10	3.1017	3.1127	3.1267	3.1477	3.1757	3.2109	3.2532	3.3028	3.3597	3.4239
435.96	3.0751	3.0860	3.0998	3.1205	3.1481	3.1828	3.2245	3.2734	3.3294	3.3927
441.60	3.0683	3.0791	3.0929	3.1135	3.1411	3.1756	3.2172	3.2658	3.3217	3.3847
457.90	3.0501	3.0609	3.0745	3.0949	3.1222	3.1564	3.1975	3.2457	3.3009	3.3634
488.00	3.0216	3.0322	3.0456	3.0657	3.0925	3.1262	3.1667	3.2141	3.2685	3.3299
514.50	3.0009	3.0113	3.0245	3.0444	3.0710	3.1043	3.1443	3.1912	3.2449	3.3055
532.00	2.9889	2.9993	3.0125	3.0322	3.0586	3.0917	3.1314	3.1780	3.2313	3.2916
546.23	2.9801	2.9905	3.0036	3.0232	3.0495	3.0823	3.1219	3.1682	3.2213	3.2812
563.20	2.9706	2.9808	2.9938	3.0134	3.0395	3.0722	3.1116	3.1576	3.2104	3.2700
594.10	2.9553	2.9655	2.9784	2.9978	3.0236	3.0561	3.0951	3.1407	3.1931	3.2521
611.90	2.9476	2.9577	2.9706	2.9899	3.0156	3.0479	3.0868	3.1322	3.1843	3.2431
632.80	2.9394	2.9495	2.9623	2.9815	3.0071	3.0393	3.0779	3.1231	3.1750	3.2335
647.10	2.9342	2.9443	2.9571	2.9762	3.0018	3.0338	3.0724	3.1175	3.1692	3.2275
670.00	2.9267	2.9367	2.9494	2.9685	2.9940	3.0259	3.0643	3.1092	3.1606	3.2187
694.30	2.9196	2.9295	2.9422	2.9612	2.9866	3.0183	3.0566	3.1013	3.1525	3.2103
725.00	2.9116	2.9215	2.9341	2.9530	2.9783	3.0099	3.0479	3.0924	3.1434	3.2010
754.00	2.9049	2.9148	2.9274	2.9462	2.9714	3.0029	3.0408	3.0851	3.1359	3.1932
785.00	2.8987	2.9085	2.9210	2.9398	2.9649	2.9963	3.0340	3.0782	3.1288	3.1859
800.00	2.8959	2.9058	2.9182	2.9370	2.9620	2.9933	3.0310	3.0751	3.1257	3.1827
836.00	2.8899	2.8997	2.9121	2.9308	2.9557	2.9870	3.0245	3.0685	3.1188	3.1756
876.00	2.8840	2.8938	2.9062	2.9248	2.9497	2.9808	3.0183	3.0621	3.1122	3.1688
904.00	2.8804	2.8902	2.9026	2.9211	2.9460	2.9770	3.0144	3.0581	3.1081	3.1646
911.28	2.8795	2.8893	2.9017	2.9202	2.9450	2.9761	3.0134	3.0571	3.1071	3.1636
946.00	2.8756	2.8854	2.8977	2.9162	2.9410	2.9719	3.0092	3.0527	3.1027	3.1590
975.00	2.8726	2.8824	2.8947	2.9132	2.9379	2.9688	3.0060	3.0495	3.0993	3.1555
1000.00	2.8703	2.8800	2.8923	2.9108	2.9354	2.9663	3.0035	3.0469	3.0967	3.1528
1064.00	2.8650	2.8747	2.8870	2.9054	2.9300	2.9608	2.9978	3.0411	3.0907	3.1467
1106.00	2.8621	2.8718	2.8840	2.9024	2.9269	2.9576	2.9946	3.0378	3.0873	3.1432
1152.00	2.8592	2.8689	2.8811	2.8994	2.9239	2.9546	2.9915	3.0347	3.0841	3.1399
1185.00	2.8574	2.8670	2.8792	2.8975	2.9220	2.9527	2.9895	3.0326	3.0820	3.1377
1225.00	2.8553	2.8650	2.8771	2.8955	2.9199	2.9505	2.9873	3.0304	3.0797	3.1353
1275.00	2.8530	2.8626	2.8748	2.8931	2.9175	2.9481	2.9848	3.0278	3.0771	3.1326
1320.00	2.8512	2.8608	2.8730	2.8912	2.9156	2.9462	2.9829	3.0258	3.0750	3.1305
Static	2.8258	2.8353	2.8473	2.8653	2.8893	2.9194	2.9555	2.9978	3.0463	3.1009
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TABLE T13. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of D₂ for v=0.

$\lambda(\text{nm})$	$\langle \gamma angle_{00,00}$	$\langle \gamma angle_{00,02}$	$\langle \gamma angle_{01,03}$	$\langle \gamma angle_{02,04}$	$\langle \gamma angle_{03,05}$	$\langle \gamma angle_{04,06}$	$\langle \gamma angle_{05,07}$	$\langle \gamma angle_{06,08}$	$\langle \gamma angle_{07,09}$	$\langle \gamma angle_{08,010}$
182.26	3.0053	3.0160	3.0301	3.0514	3.0799	3.1157	3.1589	3.2096	3.2680	3.3344
193.00	2.8470	2.8568	2.8698	2.8894	2.9156	2.9485	2.9882	3.0347	3.0883	3.1491
213.00	2.6400	2.6488	2.6604	2.6778	2.7011	2.7304	2.7656	2.8070	2.8546	2.9084
222.00	2.5714	2.5798	2.5909	2.6077	2.6301	2.6582	2.6920	2.7317	2.7773	2.8290
224.30	2.5556	2.5640	2.5750	2.5916	2.6138	2.6416	2.6752	2.7145	2.7597	2.8108
235.00	2.4904	2.4984	2.5090	2.5250	2.5463	2.5730	2.6053	2.6430	2.6864	2.7355
248.00	2.4254	2.4331	2.4433	2.4586	2.4791	2.5048	2.5357	2.5719	2.6135	2.6606
266.00	2.3545	2.3618	2.3716	2.3862	2.4058	2.4303	2.4599	2.4945	2.5342	2.5791
275.36	2.3241	2.3314	2.3409	2.3553	2.3745	2.3985	2.4275	2.4614	2.5003	2.5443
285.00	2.2966	2.3037	2.3131	2.3272	2.3461	2.3697	2.3981	2.4314	2.4696	2.5128
308.00	2.2429	2.2498	2.2588	2.2725	2.2906	2.3134	2.3408	2.3729	2.4097	2.4513
325.00	2.2115	2.2182	2.2270	2.2404	2.2582	2.2805	2.3073	2.3387	2.3747	2.4154
334.24	2.1966	2.2033	2.2120	2.2252	2.2428	2.2649	2.2915	2.3225	2.3582	2.3984
337.10	2.1923	2.1989	2.2077	2.2208	2.2384	2.2604	2.2869	2.3178	2.3534	2.3935
347.00	2.1783	2.1849	2.1935	2.2066	2.2239	2.2457	2.2719	2.3026	2.3378	2.3775
351.00	2.1730	2.1796	2.1882	2.2012	2.2185	2.2402	2.2663	2.2969	2.3319	2.3715
355.00	2.1679	2.1744	2.1831	2.1960	2.2133	2.2349	2.2609	2.2913	2.3263	2.3657
385.15	2.1351	2.1415	2.1499	2.1625	2.1794	2.2005	2.2259	2.2557	2.2898	2.3283
407.90	2.1155	2.1217	2.1300	2.1425	2.1591	2.1800	2.2050	2.2343	2.2679	2.3059
416.10	2.1092	2.1155	2.1237	2.1361	2.1527	2.1734	2.1984	2.2276	2.2610	2.2988
435.96	2.0957	2.1019	2.1100	2.1223	2.1387	2.1593	2.1840	2.2129	2.2460	2.2834
441.60	2.0922	2.0983	2.1065	2.1188	2.1351	2.1556	2.1802	2.2091	2.2421	2.2794
457.90	2.0828	2.0890	2.0971	2.1092	2.1255	2.1458	2.1703	2.1989	2.2317	2.2688
488.00	2.0682	2.0742	2.0822	2.0943	2.1104	2.1305	2.1547	2.1830	2.2155	2.2521
514.50	2.0574	2.0635	2.0714	2.0834	2.0993	2.1193	2.1433	2.1714	2.2036	2.2399
532.00	2.0513	2.0572	2.0652	2.0771	2.0929	2.1128	2.1367	2.1647	2.1967	2.2329
546.23	2.0467	2.0527	2.0606	2.0724	2.0882	2.1081	2.1319	2.1597	2.1917	2.2277
563.20	2.0417	2.0477	2.0555	2.0673	2.0831	2.1028	2.1266	2.1543	2.1861	2.2220
594.10	2.0338	2.0397	2.0475	2.0592	2.0749	2.0945	2.1181	2.1457	2.1773	2.2130
611.90	2.0297	2.0356	2.0434	2.0551	2.0708	2.0903	2.1139	2.1414	2.1729	2.2084
632.80	2.0255	2.0313	2.0391	2.0508	2.0664	2.0859	2.1093	2.1367	2.1681	2.2036
647.10	2.0228	2.0286	2.0364	2.0480	2.0636	2.0831	2.1065	2.1338	2.1652	2.2005
670.00	2.0188	2.0247	2.0324	2.0440	2.0595	2.0789	2.1023	2.1296	2.1608	2.1961
694.30	2.0151	2.0209	2.0286	2.0402	2.0557	2.0750	2.0983	2.1255	2.1567	2.1918
725.00	2.0109	2.0167	2.0244	2.0360	2.0514	2.0707	2.0938	2.1210	2.1520	2.1871
754.00	2.0074	2.0132	2.0209	2.0324	2.0478	2.0670	2.0901	2.1172	2.1482	2.1831
785.00	2.0041	2.0099	2.0176	2.0291	2.0444	2.0636	2.0867	2.1136	2.1445	2.1794
800.00	2.0027	2.0085	2.0161	2.0276	2.0429	2.0621	2.0851	2.1120	2.1429	2.1777
836.00	1.9995	2.0053	2.0129	2.0243	2.0396	2.0587	2.0817	2.1086	2.1394	2.1741
876.00	1.9964	2.0022	2.0098	2.0212	2.0365	2.0555	2.0785	2.1053	2.1360	2.1707
904.00	1.9945	2.0003	2.0079	2.0193	2.0345	2.0536	2.0765	2.1032	2.1339	2.1685
911.28	1.9941	1.9998	2.0074	2.0188	2.0340	2.0531	2.0760	2.1027	2.1334	2.1680
946.00	1.9920	1.9977	2.0053	2.0167	2.0319	2.0509	2.0738	2.1005	2.1311	2.1656
975.00	1.9904	1.9962	2.0037	2.0151	2.0303	2.0493	2.0721	2.0988	2.1294	2.1639
1000.00	1.9892	1.9949	2.0025	2.0138	2.0290	2.0480	2.0708	2.0974	2.1280	2.1625
1064.00	1.9864	1.9921	1.9997	2.0110	2.0261	2.0451	2.0678	2.0944	2.1249	2.1593
1106.00	1.9849	1.9906	1.9981	2.0094	2.0245	2.0434	2.0662	2.0928	2.1232	2.1575
1152.00	1.9833	1.9890	1.9966	2.0079	2.0230	2.0419	2.0646	2.0911	2.1215	2.1558
1185.00	1.9824	1.9881	1.9956	2.0069	2.0220	2.0408	2.0635	2.0901	2.1204	2.1547
1225.00	1.9813	1.9870	1.9945	2.0058	2.0208	2.0397	2.0624	2.0889	2.1192	2.1535
1275.00	1.9801	1.9858	1.9933	2.0045	2.0196	2.0384	2.0611	2.0876	2.1179	2.1521
1320.00	1.9791	1.9848	1.9923	2.0036	2.0186	2.0374	2.0601	2.0865	2.1168	2.1510
Static	1.9656	1.9713	1.9787	1.9898	2.0047	2.0234	2.0458	2.0719	2.1019	2.1358

TABLE T14. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} | \gamma | \psi_{v',J'} \rangle$ of D₂ for v=1.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$											
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\lambda(\text{nm})$	$\langle \gamma \rangle_{10,10}$	$\langle \gamma angle_{10,12}$	$\langle \gamma angle_{11,13}$	$\langle \gamma angle_{12,14}$	$\langle \gamma \rangle_{13,15}$	$\langle \gamma \rangle_{14,16}$	$\langle \gamma \rangle_{15,17}$	$\langle \gamma angle_{16,18}$	$\langle \gamma angle_{17,19}$	$\langle \gamma angle_{18,110}$
	182.26	3.7238	3.7365	3.7531	3.7782	3.8117	3.8538	3.9047	3.9646	4.0335	4.1119
212.00 3.1977 3.2077 3.2208 3.2405 3.2668 3.2998 3.3366 3.3489 3.3609 222.00 3.0155 3.1010 3.1235 3.1242 3.1675 3.2366 3.2810 3.33075 3.3047 235.00 2.8988 2.9978 3.0066 3.0273 3.0690 3.0275 3.0605 3.1063 3.1581 266.00 2.8982 2.9078 2.9190 2.8586 2.8850 2.9172 2.9552 2.9983 3.0473 275.36 2.7610 2.7689 2.7731 2.7414 2.7660 2.7737 2.7237 2.7315 2.7417 2.7661 2.6683 2.6613 2.7012 2.8377 2.809 2.8756 325.00 2.6547 2.6683 2.6613 2.6637 2.6841 2.7717 2.7575 2.7887 37.10 2.5676 2.6579 2.5677 2.6623 2.6903 2.6731 2.6890 2.773 2.7775 2.7351 2.7775 2.7351 2.7775	193.00	3.4929	3.5044	3.5195	3.5421	3.5724	3.6104	3.6562	3.7101	3.7722	3.8426
222.00 3.1015 3.1110 3.1235 3.1422 3.1075 3.2970 3.3211 3.3211 3.3211 3.3211 3.3270 3.3047 235.00 2.9888 2.9978 3.0096 3.0235 3.0609 3.0805 3.1161 3.2062 3.2061 248.00 2.8892 2.9078 2.1901 2.9355 2.9584 2.9868 3.0217 3.0605 3.1063 3.1581 275.36 2.7610 2.7689 2.7733 2.7449 2.8152 2.6681 2.6687 2.6685 2.6681 2.7074 2.8029 2.8371 2.8698 2.9112 2.9579 308.00 2.6542 2.6681 2.6627 2.6784 2.6637 2.6640 2.7174 2.7576 2.7440 2.7573 2.7774 3.8097 3.3017 3.351 3.7775 3.3017 3.3511 3.5151 2.5663 2.6641 2.7774 2.7657 2.7740 2.7573 2.7774 2.7657 2.7774 2.7657 2.77740 2.7612 2.7	213.00	3.1977	3.2077	3.2208	3.2405	3.2668	3.2998	3.3396	3.3863	3.4399	3.5008
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	222.00	3.1015	3.1110	3.1235	3.1422	3.1673	3.1987	3.2366	3.2810	3.3321	3.3899
225.00 2.9888 2.9978 3.0096 3.0207 3.0805 3.1162 3.1581 3.0063 3.1581 266.00 2.8092 2.8103 2.8209 2.8369 2.8850 2.9172 2.9500 2.9983 3.0473 275.36 2.7610 2.7689 2.7733 2.7417 2.7569 2.9774 2.8029 2.8374 2.8098 2.9112 2.9579 308.00 2.7537 2.7610 2.6687 2.6685 2.6681 2.7774 2.8029 2.8377 2.8698 2.9112 2.8599 2.6583 2.6697 2.7117 2.8052 3.7607 2.7240 2.7612 2.8052 347.00 2.5543 2.5071 2.5101 2.5644 2.6171 2.5731 2.7775 3.510 2.5579 2.6702 2.5633 2.6612 2.6443 2.6613 2.6451 2.7178 2.7731 2.7718 355.00 2.5579 2.5670 2.5670 2.5643 2.5761 2.6453 2.6412 2.4453 2.4612 <td>224.30</td> <td>3.0795</td> <td>3.0889</td> <td>3.1013</td> <td>3.1198</td> <td>3.1446</td> <td>3.1756</td> <td>3.2131</td> <td>3.2570</td> <td>3.3075</td> <td>3.3647</td>	224.30	3.0795	3.0889	3.1013	3.1198	3.1446	3.1756	3.2131	3.2570	3.3075	3.3647
248.00 2.8902 2.9078 2.9190 2.9359 2.9864 2.9866 3.077 3.0605 3.1063 3.1581 226.00 2.8022 2.8103 2.2799 2.8769 2.8783 2.8608 2.9172 2.9550 2.9553 3.0073 225.00 2.7315 2.7117 2.7769 2.7774 2.8099 2.8137 2.8698 2.9112 2.9579 308.00 2.6512 2.6631 2.6681 2.7027 2.7752 2.7753 2.7814 2.8877 337.10 2.5643 2.6063 2.6077 2.6182 2.6382 2.6633 2.6077 2.7761 2.7814 2.8977 337.10 2.5647 2.5779 2.5670 2.5674 2.5769 2.671 2.6798 2.7733 2.7793 355.00 2.5570 2.5674 2.5678 2.5084 2.5673 2.6037 2.6037 2.6037 2.6037 2.673 2.6337 2.6735 355.00 2.4579 2.4679 2.4583 <	235.00	2.9888	2.9978	3.0096	3.0273	3.0509	3.0805	3.1162	3.1581	3.2062	3.2606
266.00 2.8022 2.8169 2.8783 2.8850 2.9772 2.9550 2.9983 3.0473 275.36 2.7793 2.7694 2.8158 2.8419 2.9772 2.9525 3.0003 285.00 2.7337 2.7315 2.7173 2.7569 2.7774 2.8029 2.8376 2.8098 2.9112 2.9579 335.00 2.6697 2.6685 2.6681 2.7071 2.7212 2.7661 2.7621 2.7621 2.8052 334.24 2.5963 2.6607 2.6198 2.6583 2.6633 2.6071 2.7551 2.7775 351.00 2.5576 2.6407 2.5790 2.6802 2.6633 2.6633 2.6899 2.7273 2.7695 355.00 2.55070 2.5610 2.5676 2.6602 2.6637 2.6833 2.6715 2.7118 385.15 2.5071 2.5140 2.5483 2.5076 2.6638 2.6737 2.6033 2.6715 2.7198 385.0 2.4478 <td< td=""><td>248.00</td><td>2.8992</td><td>2.9078</td><td>2.9190</td><td>2.9359</td><td>2.9584</td><td>2.9866</td><td>3.0207</td><td>3.0605</td><td>3.1063</td><td>3.1581</td></td<>	248.00	2.8992	2.9078	2.9190	2.9359	2.9584	2.9866	3.0207	3.0605	3.1063	3.1581
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	266.00	2.8022	2.8103	2.8209	2.8369	2.8583	2.8850	2.9172	2.9550	2.9983	3.0473
285.00 2.7337 2.7315 2.7417 2.7569 2.78774 2.8029 2.8377 2.8088 2.9112 2.9676 308.00 2.6612 2.6587 2.6685 2.6481 2.7774 2.8376 2.7912 2.7817 2.7912 2.7812 2.7912 2.7812 2.7912 2.7812 2.7812 2.7812 2.7812 2.7812 2.7812 2.7812 2.7812 2.7851 2.7811 2.28052 347.00 2.5846 2.5717 2.5810 2.5877 2.6062 2.6294 2.6573 2.6892 2.7718 2.7718 2.7718 351.00 2.5576 2.5617 2.5670 2.5670 2.5877 2.6062 2.6294 2.6573 2.6892 2.7198 2.7118 365.15 2.5071 2.5140 2.5292 2.5434 2.5761 2.6072 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6437 2.6444 2.6537 2	275.36	2.7610	2.7689	2.7793	2.7949	2.8158	2.8419	2.8734	2.9102	2.9525	3,0003
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	285.00	2.7237	2.7315	2.7417	2.7569	2.7774	2.8029	2.8337	2.8698	2.9112	2.9579
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	308.00	2.6512	2.6587	2.6685	2.6831	2.7027	2.7272	2.7567	2.7912	2.8309	2.8756
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	325.00	2.6090	2.6163	2.6258	2.6401	2.6592	2.6831	2.7118	2.7455	2.7841	2.8277
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	334.24	2.5891	2.5963	2.6057	2.6198	2.6387	2.6623	2.6907	2.7240	2.7621	2.8052
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	337.10	2.5834	2.5905	2.5999	2.6140	2.6328	2.6563	2.6846	2.7177	2.7557	2.7987
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	347.00	2.5646	2.5717	2.5810	2.5949	2.6135	2.6368	2.6647	2.6975	2.7351	2.7775
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	351.00	2.5576	2.5647	2.5739	2.5877	2.6062	2.6294	2.6573	2.6899	2.7273	2.7695
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	355.00	2.5508	2.5579	2.5670	2.5808	2.5993	2.6223	2.6501	2.6825	2.7198	2.7618
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	385.15	2.5071	2.5140	2.5229	2.5364	2.5543	2.5767	2.6037	2.6353	2.6715	2.7124
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	407.90	2.4811	2.4878	2.4966	2.5098	2.5274	2.5495	2.5761	2.6072	2.6428	2.6830
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	416.10	2.4728	2.4795	2.4883	2.5014	2.5189	2.5409	2.5673	2.5982	2.6337	2.6736
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	435.96	2.4549	2.4615	2.4701	2.4831	2.5005	2.5222	2.5483	2.5789	2.6139	2.6534
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	441.60	2.4502	2.4569	2.4655	2.4784	2.4957	2.5174	2.5434	2.5739	2.6088	2.6482
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	457.90	2.4379	2.4445	2.4530	2.4659	2.4831	2.5045	2.5304	2.5606	2.5952	2.6343
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	488.00	2.4185	2.4250	2.4335	2.4462	2.4631	2.4843	2.5099	2.5397	2.5739	2.6125
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	514.50	2.4044	2.4108	2.4192	2.4318	2.4486	2.4696	2.4949	2.5244	2.5583	2.5965
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	532.00	2.3963	2.4027	2.4110	2.4235	2.4402	2.4611	2.4863	2.5157	2.5494	2.5874
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	546.23	2.3903	2.3966	2.4050	2.4174	2.4340	2.4549	2.4799	2.5092	2.5428	2.5806
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	563.20	2.3837	2.3901	2.3983	2.4108	2.4273	2.4481	2.4730	2.5021	2.5355	2.5732
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	594.10	2.3733	2.3796	2.3878	2.4001	2.4166	2.4372	2.4619	2.4909	2.5241	2.5615
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	611.90	2.3680	2.3743	2.3825	2.3948	2.4111	2.4317	2.4563	2.4852	2.5182	2.5555
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	632.80	2.3624	2.3686	2.3768	2.3890	2.4054	2.4258	2.4504	2.4791	2.5121	2.5492
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	647.10	2.3589	2.3651	2.3732	2.3855	2.4018	2.4222	2.4467	2.4754	2.5082	2.5453
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	670.00	2.3537	2.3599	2.3680	2.3802	2.3964	2.4168	2.4412	2.4698	2.5025	2.5395
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	694.30	2.3488	2.3550	2.3631	2.3752	2.3914	2.4117	2.4360	2.4645	2.4971	2.5339
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	725.00	2.3433	2.3495	2.3576	2.3696	2.3858	2.4060	2.4302	2.4586	2.4911	2.5278
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	754.00	2.3388	2.3449	2.3530	2.3650	2.3811	2.4012	2.4254	2.4537	2.4861	2.5226
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	785.00	2.3345	2.3406	2.3486	2.3606	2.3766	2.3967	2.4208	2.4490	2.4814	2.5178
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	800.00	2.3326	2.3387	2.3467	2.3587	2.3747	2.3947	2.4188	2.4470	2.4793	2.5157
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	836.00	2.3284	2.3345	2.3425	2.3545	2.3704	2.3904	2.4144	2.4425	2.4747	2.5110
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	876.00	2.3244	2.3305	2.3384	2.3504	2.3663	2.3862	2.4102	2.4382	2.4703	2.5065
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	904.00	2.3219	2.3280	2.3359	2.3478	2.3637	2.3837	2.4076	2.4355	2.4676	2.5037
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	911.28	2.3213	2.3274	2.3353	2.3472	2.3631	2.3830	2.4069	2.4349	2.4669	2.5030
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	946.00	2.3186	2.3247	2.3326	2.3445	2.3603	2.3802	2.4041	2.4320	2.4639	2.5000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	975.00	2.3165	2.3226	2.3305	2.3424	2.3582	2.3781	2.4019	2.4298	2.4617	2.4977
1064.002.31132.31742.32522.33712.35282.37262.39642.42412.45592.49181106.002.30932.31532.32322.33502.35082.37052.39422.42192.45372.48951152.002.30732.31332.32122.33302.34872.36842.39212.41982.45152.48731185.002.30602.31202.31992.33172.34742.36712.39082.41842.45012.48881225.002.30462.31062.31852.33022.34592.36562.38932.41692.44852.48421275.002.30302.30902.31692.32862.34432.36402.38762.41522.44682.48251320.002.30172.30782.31562.32732.34302.36272.38632.41382.44542.4810Static2.28422.29012.29792.30952.32502.34442.36772.39492.42612.4613	1000.00	2.3149	2.3210	2.3289	2.3407	2.3566	2.3764	2.4002	2.4280	2.4599	2.4958
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1064.00	2.3113	2.3174	2.3252	2.3371	2.3528	2.3726	2.3964	2.4241	2.4559	2.4918
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1106.00	2.3093	2.3153	2.3232	2.3350	2.3508	2.3705	2.3942	2.4219	2.4537	2.4895
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1152.00	2.3073	2.3133	2.3212	2.3330	2.3487	2.3684	2.3921	2.4198	2.4515	2.4873
1225.00 2.3046 2.3106 2.3185 2.3302 2.3459 2.3656 2.3893 2.4169 2.4485 2.4842 1275.00 2.3030 2.3090 2.3169 2.3286 2.3443 2.3640 2.3876 2.4152 2.4468 2.4825 1320.00 2.3017 2.3078 2.3156 2.3273 2.3430 2.3627 2.3863 2.4138 2.4454 2.4810 Static 2.2842 2.2901 2.2979 2.3095 2.3250 2.3444 2.3677 2.3949 2.4261 2.4613	1185.00	2.3060	2.3120	2.3199	2.3317	2.3474	2.3671	2.3908	2.4184	2.4501	2.4858
1275.00 2.3030 2.3090 2.3169 2.3286 2.3443 2.3640 2.3876 2.4152 2.468 2.4825 1320.00 2.3017 2.3078 2.3156 2.3273 2.3430 2.3627 2.3863 2.4138 2.4454 2.4810 Static 2.2842 2.2901 2.2979 2.3095 2.3250 2.3444 2.3677 2.3949 2.4261 2.4613	1225.00	2.3046	2.3106	2.3185	2.3302	2.3459	2.3656	2.3893	2.4169	2.4485	2.4842
1320.00 2.3017 2.3078 2.3156 2.3273 2.3430 2.3627 2.3863 2.4138 2.4454 2.4810 Static 2.2842 2.2901 2.2979 2.3095 2.3250 2.3444 2.3677 2.3949 2.4261 2.4613	1275.00	2.3030	2.3090	2.3169	2.3286	2.3443	2.3640	2.3876	2.4152	2.4468	2.4825
Static 2.2842 2.2901 2.2979 2.3095 2.3250 2.3444 2.3677 2.3949 2.4261 2.4613	1320.00	2.3017	2.3078	2.3156	2.3273	2.3430	2.3627	2.3863	2.4138	2.4454	2.4810
	Static	2.2842	2.2901	2.2979	2.3095	2.3250	2.3444	2.3677	2.3949	2.4261	2.4613

TABLE T15. Polarizability anisotropy matrix elements $\langle \gamma \rangle_{vJ,v'J'} \equiv \langle \psi_{v,J} \gamma \psi_{v',J'} \rangle$ of D ₂ for v=	=2.
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	()	()	()	()	()	()	()	()	()	()
$\lambda(\text{nm})$	$\langle \gamma \rangle_{20,20}$	$\langle \gamma angle_{20,22}$	$\langle \gamma \rangle_{21,23}$	$\langle \gamma \rangle_{22,24}$	$\langle \gamma \rangle_{23,25}$	$\langle \gamma \rangle_{24,26}$	$\langle \gamma \rangle_{25,27}$	$\langle \gamma \rangle_{26,28}$	$\langle \gamma \rangle_{27,29}$	$\langle \gamma \rangle_{28,210}$
182.26	4.5704	4.5855	4.6050	4.6345	4.6740	4.7236	4.7835	4.8541	4.9354	5.0279
193.00	4.2424	4.2558	4.2731	4.2992	4.3341	4.3779	4.4308	4.4929	4.5646	4.6459
213.00	3.8322	3.8436	3.8582	3.8803	3.9098	3.9468	3.9914	4.0438	4.1041	4.1724
222.00	3.7006	3.7113	3.7252	3.7460	3.7738	3.8088	3.8509	3.9003	3.9571	4.0215
224.30	3.6707	3.6813	3.6950	3.7155	3.7430	3.7775	3.8190	3.8678	3.9238	3.9873
235.00	3.5479	3.5580	3.5709	3.5904	3.6163	3.6489	3.6882	3.7343	3.7872	3.8471
248.00	3.4276	3.4370	3.4493	3.4677	3.4922	3.5230	3.5601	3.6036	3.6535	3.7100
266.00	3.2981	3.3071	3.3186	3.3358	3.3589	3.3878	3.4226	3.4634	3.5102	3.5631
275.36	3.2435	3.2522	3.2634	3.2802	3.3026	3.3308	3.3646	3.4043	3.4498	3.5013
285.00	3.1943	3.2027	3.2137	3.2300	3.2519	3.2794	3.3124	3.3511	3.3954	3.4456
308.00	3.0990	3.1070	3.1174	3.1330	3.1539	3.1800	3.2114	3.2482	3.2904	3.3380
325.00	3.0436	3.0515	3.0616	3.0767	3.0970	3.1223	3.1528	3.1885	3.2295	3.2757
334.24	3.0177	3.0255	3.0354	3.0503	3.0703	3.0953	3.1254	3.1606	3.2009	3.2465
337.10	3.0102	3.0179	3.0278	3.0427	3.0626	3.0875	3.1174	3.1525	3.1927	3.2380
347.00	2.9858	2.9934	3.0032	3.0179	3.0375	3.0621	3.0916	3.1262	3.1658	3.2106
351.00	2.9766	2.9842	2.9939	3.0085	3.0281	3.0525	3.0819	3.1163	3.1558	3.2003
355.00	2.9678	2.9753	2.9850	2.9996	3.0190	3.0433	3.0726	3.1068	3.1461	3.1904
385.15	2.9111	2.9184	2.9278	2.9419	2.9607	2.9843	3.0126	3.0458	3.0838	3.1267
407.90	2.8773	2.8845	2.8937	2.9075	2.9260	2.9491	2.9770	3.0095	3.0468	3.0888
416.10	2.8666	2.8738	2.8829	2.8967	2.9150	2.9380	2.9657	2.9980	3.0351	3.0769
435.96	2.8435	2.8505	2.8596	2.8731	2.8913	2.9139	2.9412	2.9731	3.0097	3.0509
441.60	2.8375	2.8445	2.8536	2.8671	2.8851	2.9077	2.9349	2.9667	3.0031	3.0443
457.90	2.8216	2.8286	2.8375	2.8509	2.8688	2.8912	2.9181	2.9496	2.9857	3.0265
488.00	2.7967	2.8036	2.8124	2.8256	2.8432	2.8653	2.8918	2.9229	2.9584	2.9986
514.50	2.7785	2.7853	2.7940	2.8071	2.8245	2.8464	2.8727	2.9034	2.9385	2.9782
532.00	2.7681	2.7748	2.7835	2.7965	2.8138	2.8355	2.8616	2.8922	2.9271	2.9666
546.23	2.7604	2.7671	2.7757	2.7886	2.8059	2.8275	2.8535	2.8839	2.9187	2.9579
563.20	2.7520	2.7587	2.7672	2.7801	2.7973	2.8188	2.8446	2.8749	2.9095	2.9485
594.10	2.7386	2.7452	2.7537	2.7665	2.7835	2.8049	2.8305	2.8605	2.8948	2.9336
611.90	2.7318	2.7384	2.7409	2.7596	2.7700	2.7978	2.8234	2.8032	2.8875	2.9260
632.80	2.7240	2.7312	2.7390	2.7323	2.7692	2.7904	2.8158	2.8455	2.8790	2.9180
647.10	2.7201	2.7207	2.7301	2.7477	2.7040	2.1801	2.8110	2.8407	2.8/4/	2.9130
604.20	2.7155	2.7201	2.7204	2.7410	2.7576	2.1100	2.6041	2.0000	2.6074	2.9030
725.00	2.7072	2.7138	2.7221 2.7150	2.7340	2.7314	2.7725	2.7975	2.8209	2.8000	2.8980
725.00	2.7002	2.7007	2.7150	2.7215	2.1442	2.7650	2.7901	2.0194	2.8529	2.8908
795.00	2.0944	2.7009	2.7092	2.7210	2.1362	2.7590	2.7639	2.0131	2.8400	2.0043
800.00	2.0885	2.0900	2.7030 2 7011	2.7100	2.7320	2.7502 2.7507	2.7756	2.8012	2.8400	2.8754
836.00	2.0803	2.0325 2.6876	2.7011	2.7133 2 7081	2.7300	2.7307	2.7700	2.3040	2.8373	2.8754
876.00	2.6760	2.6824	2.6906	2.7001	2.7240	2.7402	2.7700	2.7935	2.8265	2.8638
904.00	2.6729	2.6793	2.6300	2.1025	2.7154	2.7366	2.7612	2.7900	2.8230	2.8602
911 28	2.6721	2.6785	2.6867	2.6989	2 7153	2.7358	2.7604	2 7892	2.8230 2.8222	2.8594
946.00	2.6686	2.6750	2.6832	2.6954	2.7117	2.7322	2.7568	2.7855	2.8184	2.8555
975.00	2.6660	2.6724	2.6805	2.6928	2 7091	2 7295	2.7540	2 7827	2.8156	2.8526
1000.00	2.6640	2.6703	2.6785	2.6907	2,7070	2.7274	2.7519	2.7805	2.8133	2.8503
1064.00	2.6593	2.6657	2.6738	2.6860	2,7022	2 7226	2.7470	2,7756	2.8083	2.8452
1106.00	2.6567	2.6631	2.6712	2.6833	2.6995	2.7199	2.7443	2.7728	2.8054	2.8423
1152.00	2.6542	2.6605	2.6686	2.6808	2.6970	2.7172	2,7416	2.7701	2.8027	2,8394
1185.00	2.6526	2.6589	2.6670	2.6791	2.6953	2.7155	2.7399	2.7683	2.8009	2.8376
1225.00	2.6508	2.6571	2.6652	2.6773	2.6934	2.7137	2.7380	2.7664	2.7989	2.8356
1275.00	2.6488	2.6551	2.6631	2.6752	2.6914	2.7116	2.7359	2.7642	2.7967	2.8334
1320.00	2.6472	2.6535	2.6615	2.6736	2.6897	2.7099	2.7342	2.7625	2.7950	2.8316
Static	2.6248	2.6310	2.6390	2.6509	2.6668	2.6867	2.7106	2.7386	2.7706	2.8067

TABLE T16. Conversion factors for polarizability.

Atomic units ^a		Conversion factor	Resulting units
$ \begin{array}{c} 1 \ e^2 a_0^2 E_h^{-1} \\ 1 \ e^2 a_0^2 E_h^{-1} \\ 1 \ e^2 a_0^2 E_h^{-1} \end{array} \\ \end{array} $	$\begin{array}{c} \rightarrow \\ \rightarrow \\ \rightarrow \end{array}$	$\begin{array}{c} 1.648777254\times10^{-41}\\ 1.481847096\times10^{-1}\\ 1.481847096\times10^{-25} \end{array}$	$\stackrel{\mathrm{C}^2\mathrm{m}^2\mathrm{J}^{-1}}{\overset{\mathrm{A}^3}{\mathrm{cm}^3}}$

^a With the factor of $1/4\pi\epsilon_0$ incorporated.

S3. Static polarizability components and invariants for H_2 at selected distances

TABLE T17. Static polarizability components and invariants for H₂, HD and D₂ at selected distances obtained from linear response procedures with CCSD method and a composite basis: aug-mcc-pV6Z+5×BF(8s6p)basis set. These results were obtained using the cutoff for linear dependence of AOs as 1.0×10^{-6} , the convergence criteria for SCF energy gradient set to 1.0×10^{-11} a.u., CC energy convergence criteria of 1.0×10^{-9} a.u. and response solutions convergence criteria of 1.0×10^{-7} a.u.

r	$lpha_{\perp}$	$lpha_{\parallel}$	$\bar{\alpha}$	γ
0.5	2.0624087	2.1975812	2.1074662	0.1351725
0.6	2.2859038	2.4946745	2.3554940	0.2087707
0.7	2.5277157	2.8320145	2.6291486	0.3042988
0.8	2.7857901	3.2104246	2.9273349	0.4246345
0.9	3.0583152	3.6309366	3.2491890	0.5726214
1.0	3.3436207	4.0945591	3.5939335	0.7509384
1.1	3.6401071	4.6020540	3.9607561	0.9619469
1.2	3.9460506	5.1538307	4.3486440	1.2077801
1.3	4.2597572	5.7497741	4.7564295	1.4900169
1.4	4.5794132	6.389 121 8	5.182 649 4	1.809 708 6
1.5	4.903 176 6	7.070 300 2	5.6255511	2.167 123 6
1.6	5.229 1027	7.790 806 0	6.083 003 8	2.561 703 3
1.7	5.5551379	8.547 074 3	6.5524500	2.991 936 4
1.8	5.8791890	9.3343154	7.030 897 8	3.4551264
1.9	0.1991233	10.1404130	1.014 001 2	3.947 2917
2.0	0.0120908	10.9759780	8.000 450 5	4.403 282 2
2.1	0.0177074	11.0141410 19.6507140	0.400 100 0	4.990 433 0 E E20 7EE 2
2.2	7 303 267 5	12.0507140	0.420.260.3	6 080 078 5
2.3	7.595.207.5	14 272 250 0	9.420 200 3	6 612 600 1
2.4	7 000 222 8	15.031.028.0	10 283 458 5	7 122 704 2
2.5	8 140 2428	15.0315280 15.7395870	10.2034000 10.6733575	7 500 344 2
2.7	8.351 253 9	16.3821540	11.028.220.6	8.030.900.1
2.8	8.5412287	16.9475420	11.343 333 1	8 406 313 3
2.9	8,709,382,2	17,424,939,0	11.6145678	8.715.556.8
3.0	8.855 379 0	17.8056790	11.8388123	8.950 300 0
3.1	8.9793015	18.0838460	12.0141497	9.1045445
3.2	9.0816696	18.2565260	12.1399551	9.1748564
3.3	9.1634275	18.3241210	12.2169920	9.1606935
3.4	9.2258983	18.2903290	12.2473752	9.0644307
3.5	9.2707232	18.1619020	12.2344495	8.8911788
3.6	9.2997842	17.9482030	12.1825905	8.6484188
3.7	9.3151174	17.6605850	12.0969399	8.3454676
3.8	9.3188236	17.3116900	11.9831124	7.9928664
3.9	9.3129830	16.9147210	11.8468957	7.6017380
4.0	9.2995820	16.4827570	11.6939737	7.1831750
4.2	9.2572416	15.5621860	11.358 889 7	6.304 944 4
4.4	9.204 034 2	14.633 575 0	11.013 881 1	5.429 540 8
4.6	9.148 702 8	13.756 300 0	10.684 568 5	4.607 597 2
4.8	9.0967923	12.964 991 0	10.386 191 9	3.868 198 7
5.U F 9	9.051 249 1	12.273 1880	10.125 895 4	3.223 938 9
0.Z	9.013 233 3	11.000.001.0	9.905 050 5	2.0734437
5.6	8 050 258 2	10 705 648 0	9.721.327.2	2.210 200 7
5.8	8 941 779 0	10.7550480 10.4664950	9.450.017.7	1.5305356 15247160
6.0	8 929 350 2	10.4004000	9 352 802 5	1.0247100 1.2703568
6.2	8 921 020 5	9 984 434 8	9 275 491 9	1 063 414 3
6.4	8.915 935 3	9.811 200 1	9.214 356 9	0.895 264 8
6.6	8.9134031	9.6720148	9.1662737	0.7586117
6.8	8.9127388	9.5601120	9.1285299	0.6473732
7.0	8.9134785	9.4700763	9.0990111	0.5565978
7.5	8.9190761	9.3137500	9.0506341	0.3946739
8.0	8.9270472	9.2204861	9.0248602	0.2934389
8.5	8.9353130	9.1628676	9.0111645	0.2275546
9.0	8.9429734	9.1255820	9.0038429	0.1826086
9.5	8.9497258	9.1001745	8.9998754	0.1504487
10.0	8.9555337	9.0819822	8.9976832	0.1264485
10.5	8.9604685	9.0683728	8.9964366	0.1079043
11.0	8.9646412	9.0577973	8.9956932	0.0931561
11.5	8.9681716	9.0493189	8.9952207	0.0811473
12.0	8.9711730	9.0423709	8.9949056	0.0711979

S4. Development of the bond functions used in this work

The improvement in the energy of H_2 by introduction of bond functions has been studied by Wright and coworkers[2–4] who showed that employing bond functions of type 2s2p and 3s3p2d gives improved energies for H_2 . We tested the bond functions as given in Ref. 2 and 3 namely, 2s2p2d and 3s3p3d, while adding more s- and p- functions, which however, did not result in significant improvement of the polarizability. The bond functions mentioned in Ref. 2–4 were optimized only at r=1.4 a.u. for the energy of the molecule, and hence as expected they did not perform well at larger distances as shown in Fig. F1, where the difference of the invariants of static polarizability to the data given by Rychlewski[5] are plotted against the internuclear distance. In the present work, we are computing integrals up to the v=1, J=10 state and the wavefunction for the highest state diminish to zero at r=3.4 a.u., hence we need accurate polarizability at least up to this distance.



FIG. F1. The values of $\bar{\alpha} - \bar{\alpha}_{ref}$ and $\gamma - \gamma_{ref}$ for the static polarizabilities of H₂ as a function of the internuclear distance. The $\bar{\alpha}$ and γ invariants are computed with CCSD methodology using the composite aug-mcc-pV6Z+5×BF basis set. The reference values $\bar{\alpha}_{ref}$ and γ_{ref} are taken from the work of Rychlewski (Ref. 5). The basis sets is composed of aug-cc-pV6Z basis as the AO basis and the bond functions given in the legend. These bond functions were taken from the work of Wright and coworkers[2, 3] where we have added additional diffuse functions following the same ratio for the exponents as in the original work.

It seems important to investigate which types of functions (namely s-, p- or d-) are important as bond functions, and what are the appropriate size and the number of functions needed. To answer these questions, different sized s-, p- and d- functions were placed on a number of equally spaced points along the H–H bond, and the static polarizability was computed at several internuclear distances. By comparing the results with those given by Rychlewski (Ref. 5) it was found that less than 5 number of equally spaced points with bond functions do not provide all the basis functions needed for larger distances especially r>3 a.u. (see Fig. F2). Hence, we chose to place bond functions on 5 equidistant points along the internuclear distance.

Upon testing many different sized s-, p- and d- functions we found that p-functions are the most important towards the improvement of polarizability. Differently sized p-functions were then checked and optimized to obtain a 6p-function set as a good candidate (see main text for the exponents). After the p-functions, the s-functions were found to be the most relevant. It was found that the d-functions affect the polarizability values to the least degree, as shown in Fig. F4.

Since we added additional basis functions for our calculations, we checked the consistency of our results by changing the parameters controlling the cut-off for numerical linear dependence of basis functions, the convergence criteria for SCF and CCSD energies and the convergence criteria for response solutions.

• In the DALTON package, the linear dependence of basis functions is controlled within the program by computing the overlap matrix of the basis functions (also known as AO overlap matrix) and removing the eigenvectors whose eigenvalues are less than the cutoff defining the numerical linear dependence (default cutoff= 1×10^{-6}). This cutoff governs which basis functions are removed to avoid mathematically incorrect results. AOs with bond functions supply excess basis functions to be used for generating the MOs, and this check for linear dependence removes functions not needed. In our tests, the cut-off



FIG. F2. The values of $\bar{\alpha} - \bar{\alpha}_{ref}$ and $\gamma - \gamma_{ref}$ for the static polarizabilities of H₂ as a function of internuclear distance. The $\bar{\alpha}$ and γ invariants are computed with CCSD using the composite aug-mcc-pV6Z+n×BF basis set. The reference values $\bar{\alpha}_{ref}$ and γ_{ref} are taken from the work of Rychlewski (Ref. 5). The basis sets include the aug-cc-pVDZ as the AO functions and the different number of bond functions placed at *n*-equidistant points along the H–H are given in the legend.



FIG. F3. The values of $\bar{\alpha} - \bar{\alpha}_{ref}$ and $\gamma - \gamma_{ref}$ for the static polarizabilities of H₂ as a function of internuclear distance. The $\bar{\alpha}$ and γ invariants are computed with CCSD using the composite aug-mcc-pV6Z+5×BF basis set. The reference values $\bar{\alpha}_{ref}$ and γ_{ref} are taken from the work of Rychlewski (Ref. 5). Deviation observed for the 6Z+5×BF(5p), shown in violet, from the lines for larger basis at r=1.5 a.u. for $\bar{\alpha}$ and r=1.75 a.u. for γ indicates that this basis does not have enough functions for the larger internuclear distances. 6p- and larger bond functions along with 6Z AO basis show same differences at all distances indicating they give converged results since no significant departure in the differences are observed at any distance for these cases.

for linear dependence was varied within 10^{-6} to 10^{-11} to check the effect on the polarizability (see table T18). The default cutoff for linear dependence (10^{-6}) gave reproducible results up to the fourth decimal digit for both α_{\perp} and α_{\parallel} . The cut-off at $10^{-7} - 10^{-11}$ gave converged results for both the components of polarizability shown in Table T18. In the present work, the default cutoff (of 10^{-6}) been used which, however, causes a change of 1.0×10^{-5} for $\bar{\alpha}$ and 1.0×10^{-4} for γ . This effect of the cutoff for linear dependence is accounted when describing the error in the computed matrix elements.



FIG. F4. The values of $\bar{\alpha} - \bar{\alpha}_{ref}$ and $\gamma - \gamma_{ref}$ for the static polarizabilities of H₂ as a function of internuclear distance. The $\bar{\alpha}$ and γ invariants are computed with CCSD using the composite aug-mcc-pV6Z+5×BF basis set. The reference values $\bar{\alpha}_{ref}$ and γ_{ref} are taken from the work of Rychlewski (Ref. 5). This plot shows that 6p- bond functions gives similar polarizability as with larger bond-functions indicating that polarizability is nearly converged. Additional s-functions affect polarizability only by less than 0.002 a.u. across all distances, and d-functions only affect the polarizability at distances larger than 5 a.u. and only by ~0.001 a.u. or less.

TABLE T18. Change of static polarizability r=1.4 a.u. with the cutoff for linear dependence of atomic orbital basis functions when using the composite basis: aug-mcc-pV6Z+5×BF(8s6p). The following test was performed using the convergence criteria for SCF energy gradient as 1.0×10^{-11} a.u., convergence criteria for CC energy as 1.0×10^{-9} a.u. and the convergence criteria for response solutions as 1.0×10^{-7} a.u.

AO linear dependence cutoff	$lpha_\perp$	$lpha_{\parallel}$	$ar{lpha}$	γ
1.0×10^{-6}	4.5794132	6.3891218	5.1826494	1.8097086
1.0×10^{-7}	4.5794388	6.3891060	5.1826612	1.8096672
1.0×10^{-8}	4.5794388	6.3891060	5.1826612	1.8096672
1.0×10^{-9}	4.5794388	6.3891060	5.1826612	1.8096672
1.0×10^{-10}	4.5794388	6.3891060	5.1826612	1.8096672
1.0×10^{-11}	4.5794388	6.3891060	5.1826612	1.8096672

• Convergence of the wavefunctions and the respective energy was ascertained by tightening the SCF convergence criteria for the energy gradient to 10^{-11} a.u. and the CCSD energy convergence criteria to 10^{-9} a.u. The response results (for example, polarizability) were checked by tightening the convergence criteria for response solutions to 10^{-7} a.u. (see table T19). The change in the values of polarizability was found to be consistent with the set convergence criteria, indicating stable converged results and the final calculations were performed using these tightened parameters.

TABLE T19. Change of static polarizability at r=1.4 a.u. with the convergence criteria for the SCF energy gradient, CC energy and the solutions to the response equations respectively, when using the composite basis: aug-mccpV6Z+5×BF(8s6p). Two tests were performed where, (i) AO linear dependence cutoff as 1.0×10^{-6} a.u. and (ii) AO linear dependence cutoff as 1.0×10^{-11} a.u. For both the tests, the convergence criteria for the SCF energy gradient was changed from 1.0×10^{-6} to 1.0×10^{-11} a.u., convergence criteria for CC energy was two orders of magnitude larger than that for the case of SCF energy gradient while the convergence criteria for response solutions was two orders of magnitude larger than that for the case of CC energy. All numbers are in the respective a.u.

	Conve	ergence thres	hold				
AO linear dependence cutoff	SCF energy	CC energy	Linear Response	$lpha_{\perp}$	$lpha_\parallel$	$ar{lpha}$	γ
1.0×10^{-6}	1.0×10^{-6}	1.0×10^{-4}	1.0×10^{-2}	4.5808752	6.3909560	5.1842355	1.810 080 8
	1.0×10^{-7}	1.0×10^{-5}	1.0×10^{-3}	4.5795105	6.3891243	5.1827151	1.8096138
	1.0×10^{-8}	1.0×10^{-6}	1.0×10^{-4}	4.5794766	6.3891295	5.1826942	1.8096529
	1.0×10^{-9}	1.0×10^{-7}	1.0×10^{-5}	4.5794170	6.3891245	5.1826528	1.8097075
	1.0×10^{-10}	1.0×10^{-8}	1.0×10^{-6}	4.5794132	6.3891218	5.1826494	1.8097086
	1.0×10^{-11}	1.0×10^{-9}	1.0×10^{-7}	4.5794132	6.3891218	5.1826494	1.8097086
1.0×10^{-11}	1.0×10^{-6}	1.0×10^{-4}	1.0×10^{-2}	4.5809177	6.3909704	5.1842686	1.8100527
	1.0×10^{-7}	1.0×10^{-5}	1.0×10^{-3}	4.5795359	6.3891072	5.1827263	1.8095713
	1.0×10^{-8}	1.0×10^{-6}	1.0×10^{-4}	4.5795023	6.3891133	5.1827060	1.8096110
	1.0×10^{-9}	1.0×10^{-7}	1.0×10^{-5}	4.5794943	6.3891087	5.1826991	1.8096144
	1.0×10^{-10}	1.0×10^{-8}	1.0×10^{-6}	4.5794388	6.3891061	5.1826612	1.8096673
	1.0×10^{-11}	1.0×10^{-9}	1.0×10^{-7}	4.5794388	6.389 106 0	5.1826612	1.8096672

S5. Details of the numerical procedure used for the solution of the 1D Schrödinger equation

A. Introduction

Consider the Schrödinger equation

$$\Omega\psi(x) = E\psi(x) \tag{1}$$

where operator Ω is some form of differential operator representing the Hamiltonian in one dimension(say x). Let the eigenvectors be given as $\psi(x)$ while the eigenvalues as E. The objective is to obtain a solution which comprises of, the eigenvalue E and the eigenvector ψ , for a given operator Ω . Consider a finite region in x where the solution exists and is real valued. For such a region, one can consider a finite number of points in x giving us a grid of points with uniform step h. If the operator Ω can be expressed explicitly for each of these points on x, then one can map the equations onto a square matrix (described as H-matrix) where each diagonal element corresponds to the point in the finite grid on x. Eigendecomposition of this matrix would yield the left and right eigenvectors arranged in the form of square matrices and a square diagonal matrix having eigenvalues. This is the outline of the process for obtaining a solution to the Schrödinger equation. The focus then shifts to the process of mapping the differential operator Ω spanning over some finite region in x on some chosen grid points.

B. Finite difference formulae for approximating the derivative

The finite difference method for obtaining a numerical solution to the differential equations is based on the concept of using appropriate differences over a grid of points (discretization) rather than continuous derivatives (differentiation) of analytic functions. In this method, truncated Taylor series expansion at each grid point can be used to effectively compute numerical derivatives as differences shown in the following description. For a general function f(x), the central difference formula of the order h^4 (i.e. using up to the 4th-order derivative) can be derived using the Taylor series expansion about x for f(x - 2h), f(x - h), f(x), f(x+h) and f(x+2h) which are;

$$\begin{aligned} f(x-2h) &= f(x) - 2hf^{(1)}(x) + \frac{4h^2f^{(2)}(x)}{2!} - \frac{8h^3f^{(3)}(x)}{3!} + \frac{16h^4f^{(4)}(x)}{4!} - \frac{32h^5f^{(5)}(\tau_2)}{5!} \\ f(x-h) &= f(x) - hf^{(1)}(x) + \frac{h^2f^{(2)}(x)}{2!} - \frac{h^3f^{(3)}(x)}{3!} + \frac{h^4f^{(4)}(x)}{4!} - \frac{h^5f^{(5)}(\tau_1)}{5!} \\ f(x) &= f(x) + 0 + 0 + 0 + 0 \\ f(x+h) &= f(x) + hf^{(1)}(x) + \frac{h^2f^{(2)}(x)}{2!} + \frac{h^3f^{(3)}(x)}{3!} + \frac{h^4f^{(4)}(x)}{4!} + \frac{h^5f^{(5)}(\tau_1)}{5!} \\ f(x+2h) &= f(x) + 2hf^{(1)}(x) + \frac{4h^2f^{(2)}(x)}{2!} + \frac{8h^3f^{(3)}(x)}{3!} + \frac{16h^4f^{(4)}(x)}{4!} + \frac{32h^5f^{(5)}(\tau_2)}{5!} \end{aligned}$$

where τ is some point within (x - 2h) and (x + 2h). Note that the above equations have the 5th derivative term which is included for error estimation in this approximation.

Difference of the last and the first term in Eqn. 2 gives,

$$f(x+2h) - f(x-2h) = 4hf^{(1)}(x) + \frac{16h^3f^{(3)}(x)}{3!} + \frac{64h^5f^{(5)}(\tau_2)}{5!}$$
(3)

while, the difference between the second last and the second term in Eqn. 2 gives,

$$f(x+h) - f(x-h) = 2hf^{(1)}(x) + \frac{2h^3f^{(3)}(x)}{3!} + \frac{2h^5f^{(5)}(\tau_1)}{5!}$$
(4)

Subtracting Eqn. 3 from Eqn. 4 and rearranging gives,

$$-f(x+2h) + 8f(x+h) - 8f(x-h) + f(x-2h) = 12hf^{(1)} + \frac{h^5(16f^{(5)}(\tau_1) - 64f^{(5)}(\tau_2))}{120}$$
(5)

Assuming that the $f^{(5)}$ is smooth over the (x - 2h). (x + 2h) and preserves its sign over this interval, the second term in Eqn. 5 can be simplified using a common value of τ which is within the interval (x - 2h). (x + 2h), giving,

$$16f^{(5)}(\tau_1) - 64f^{(5)}(\tau_2) = -48f^{(5)}(\tau) \tag{6}$$

Using Eqn. 6, Eqn. 5 can be rewritten for $f^{(1)}$ as,

$$f^{(1)} = \frac{-f(x+2h) + 8f(x+h) - 8f(x-h) + f(x-2h)}{12h} + \frac{h^4 f^{(5)}(\tau)}{30}$$
(7)

The first term of the right hand side in the above expression is an approximation for the first derivative, where the coefficients (also known as difference quotients), namely, $\left(\frac{-1}{12h}, \frac{8}{12h}, \frac{-8}{12h}, \frac{1}{12h}\right)$ are derived algebraically for the present case. The second term of the right hand side is the truncation error. The truncation error is dependent on the step size (h) and for the first derivative it is generalized as,

$$\operatorname{Error}(h^{n}) = \frac{h^{n} f^{(n+1)}(x)}{(n+1)(n+2)}$$
(8)

Using a similar treatment, other numerical derivative approximations specifically, forward and backward difference, and various versions of asymmetric difference formulations can be obtained. It is to be noted that the expression for the truncation error will be different for each case. The process of obtaining the coefficients for the relevant derivative can also be treated as a problem of set of linear equations (for example, see section S5 C) which can be solved using a matrix equation, allowing for convenient implementation on a computer code. Formulae for numerous other kind of differences for the approximation of derivative can be found in Ref. [6, 7].

C. Matrix mathematics approach to coefficients of the terms in the finite difference method

Consider a general function f(x) whose value at f(x+h) can be written in terms of Taylor series expansion and the series can be truncated up to the 4th derivative term giving,

$$f(x+h) = f(x) + hf^{(1)}(x) + \frac{h^2 f^{(2)}(x)}{2!} + \frac{h^3 f^{(3)}(x)}{3!} + \frac{h^4 f^{(4)}(x)}{4!}$$
(9)

Consider a point x_0 around which the numerical values of $f(x_0)$ and $f(x_0 + nh)$ are available. For evaluating the derivative at x_0 the 5-point numerical derivative (an example of left handed asymmetric derivative also known as forward difference) can be employed,

$$f(x_{0}) = f(x_{0}) + 0 + 0 + 0 + 0$$

$$f(x_{0} + h) = f(x_{0}) + hf^{(1)}(x_{0}) + \frac{h^{2}f^{(2)}(x_{0})}{2!} + \frac{h^{3}f^{(3)}(x_{0})}{3!} + \frac{h^{4}f^{(4)}(x_{0})}{4!}$$

$$f(x_{0} + 2h) = f(x_{0}) + 2hf^{(1)}(x_{0}) + \frac{4h^{2}f^{(2)}(x_{0})}{2!} + \frac{8h^{3}f^{(3)}(x_{0})}{3!} + \frac{16h^{4}f^{(4)}(x_{0})}{4!}$$

$$f(x_{0} + 3h) = f(x_{0}) + 3hf^{(1)}(x_{0}) + \frac{9h^{2}f^{(2)}(x_{0})}{2!} + \frac{27h^{3}f^{(3)}(x_{0})}{3!} + \frac{8h^{4}f^{(4)}(x_{0})}{4!}$$

$$f(x_{0} + 4h) = f(x_{0}) + 4hf^{(1)}(x_{0}) + \frac{16h^{2}f^{(2)}(x_{0})}{2!} + \frac{64h^{3}f^{(3)}(x_{0})}{3!} + \frac{256h^{4}f^{(4)}(x_{0})}{4!}$$
(10)

The objective is then to obtain the required derivative in terms of appropriate coefficients $(C_0, C_1, C_2, C_3$ and $C_4)$. This can be performed by constructing a set of 5-linear equations, one each for one of the derivative and solving them to obtain the required coefficients.

Set of Eqns. 10 can be transformed into a matrix (F) where the elements are the numerical values of the Taylor series coefficients. Transpose of this matrix would arrange the coefficients such that each row corresponds to the coefficients C_0 , C_1 , C_2 , C_3 and C_4 for the derivative of a certain degree.

$$F = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 \\ 1 & 1 & \frac{1}{2} & \frac{1}{6} & \frac{1}{24} \\ 1 & 2 & 2 & \frac{8}{6} & \frac{16}{24} \\ 1 & 3 & \frac{9}{2} & \frac{27}{6} & \frac{81}{24} \\ 1 & 4 & \frac{16}{2} & \frac{64}{6} & \frac{256}{24} \end{bmatrix}$$
(11)

$$A = F^{T} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 \\ 0 & 1 & 2 & 3 & 4 \\ 0 & \frac{1}{2} & 2 & \frac{9}{2} & \frac{16}{2} \\ 0 & \frac{1}{6} & \frac{8}{6} & \frac{27}{6} & \frac{64}{6} \\ 0 & \frac{1}{24} & \frac{16}{24} & \frac{81}{24} & \frac{256}{24} \end{bmatrix}$$
(12)

$$[A]_{5\times 5}[C]_{5\times 1} = [B]_{5\times 1} \tag{13}$$

$$\begin{bmatrix} 1 & 1 & 1 & 1 & 1 \\ 0 & 1 & 2 & 3 & 4 \\ 0 & \frac{1}{2} & 2 & \frac{9}{2} & \frac{16}{2} \\ 0 & \frac{1}{6} & \frac{8}{6} & \frac{27}{6} & \frac{64}{6} \\ 0 & \frac{1}{24} & \frac{16}{24} & \frac{81}{24} & \frac{256}{24} \end{bmatrix} \begin{bmatrix} C_0 \\ C_1 \\ C_2 \\ C_3 \\ C_4 \end{bmatrix} = \begin{bmatrix} f^{(0)} \\ f^{(1)} \\ f^{(2)} \\ f^{(3)} \\ f^{(4)} \end{bmatrix}$$
(14)

Using the matrix eqn. 14 the coefficients $(C_0, C_1, C_2, C_3 \text{ and } C_4)$ can be obtained for any of the derivative by assigning it as unity in the column matrix B. Such condition(s) are shown below for the first and the second

derivative.

$$B = \begin{bmatrix} 0\\1\\0\\0\\0 \end{bmatrix} \quad \text{for first derivative; and} \quad B = \begin{bmatrix} 0\\0\\1\\0\\0 \end{bmatrix} \quad \text{for second derivative} \tag{15}$$

Matrix equation AC = B can be solved as $C = A^{-1}B$ Each coefficient has to be divided with the value of (h^n) for the specific n^{th} -order derivative, for example,

$$C: \left(\frac{C_0}{h}, \frac{C_1}{h}, \frac{C_2}{h}, \frac{C_3}{h}, \frac{C_4}{h}\right), \text{ for the first derivative and}$$
(16)

$$C: \left(\frac{C_0}{h^2}, \frac{C_1}{h^2}, \frac{C_2}{h^2}, \frac{C_3}{h^2}, \frac{C_4}{h^2}\right), \text{ for the second derivative.}$$
(17)

The explanation given above is for the 5-point forward difference. A similar technique can be used to compute the required coefficients for the backward and central difference methods.

Mapping the operator Ω on a matrix followed by eigendecomposition

As shown in the previous section, numerical derivatives can be computed by appropriately choosing 5 points when using Taylor series expansion up to the 4th degree. For the present case, the region over the one-dimensional space over which the solution of the differential equation is sought can be divided into a finite number of points, say from x_0 to x_n having step of h. For the first point (x_0) , the derivative can be described using the forward difference. For the second point (x_1) , asymmetric derivative using expansions over $f(x_1 - h)$, $f(x_1)$, $f(x_1 + h)$ $f(x_1 + 2h)$, and $f(x_1 + 3h)$ can be used. From the 3rd point (x_2) up to the $n - 2^{\text{th}}$ point symmetric derivative using expansions over $f(x_2 - 2h)$, $f(x_2 - h)$, $f(x_2)$, $f(x_2 + h)$ and $f(x_2 + 2h)$ can be employed. For the $n - 1^{\text{th}}$ point, asymmetric derivative similar to the x_1 can be used. For the very last point (x_n) , backward difference can be used. This is shown using Table T20.

TABLE T20. Taylor expansions required for computing derivative at certain point on a grid spanning from x_0 to x_n with step of h.

Point on grid		Taylor	expansions re	quired	
x_0	$f(x_0)$	$f(x_0+h)$	$f(x_0 + 2h)$	$f(x_0 + 3h)$	$f(x_0 + 4h)$
x_1	$f(x_1-h)$	$f(x_1)$	$f(x_1 + h)$	$f(x_1 + 2h)$	$f(x_1 + 3h)$
x_2	$f(x_2 - 2h)$	$f(x_2-h)$	$f(x_2)$	$f(x_2 + h)$	$f(x_2 + 2h)$
x_3	$f(x_3 - 2h)$	$f(x_3-h)$	$f(x_3)$	$f(x_3+h)$	$f(x_3 + 2h)$
÷	÷	•	:		•
x_{n-2}	$f(x_{n-2} - 2h)$	$f(x_{n-2}-h)$	$f(x_{n-2})$	$f(x_{n-2}+h)$	$f(x_{n-2} + 2h)$
x_{n-1}	$f(x_{n-1} - 3h)$	$f(x_{n-1}-2h)$	$f(x_{n-1}-h)$	$f(x_{n-1})$	$f(x_{n-1}+h)$
<i>x</i> _n	$f(x_n - 4h)$	$f(x_n - 3h)$	$f(x_n - 2h)$	$f(x_n - h)$	$f(x_n)$

As shown in the previous discussion, for each derivative required in the relevant operator, the appropriate coefficients for numerical differentiation can be computed by solving a set of linear equations. This provides us with the coefficients $(C_0, C_1, C_2, C_3 \text{ and } C_4)$ for each point x_0 to x_n . Using these coefficients the numerical derivative can be explicitly defined, as shown using the following example.

Consider the operator Ω as,

$$\Omega = \frac{\partial^2}{\partial x^2} + k(x) \simeq \frac{d^2}{dx^2} + k(x) \tag{18}$$

In Eqn. 18, the second derivative term $(\frac{d^2}{dx^2})$ can now be expressed using C_0/h^2 , C_1/h^2 , C_2/h^2 , C_3/h^2 and C_4/h^2 and the numerical value of the k(x) term is added to the respective equation. This is shown using Eqns. 19.

Following Eqns. 19, the H-matrix can be formulated where the derivative term takes 5 columns, which are asymmetric (around the diagonal) for the first and last two rows, while symmetric for the other rows. The k(x) term is added to the diagonal term. This is shown using Fig. F5. Eigendecomposition of the resulting H-matrix gives three square matrices (F6), two for the eigenvectors and one for the eigenvalues.

/	、 、						-									
									1							
										0	0	(C_0/h^2)	(C_1/h^2)	$(C_2/h^2) \ +k(x_4)$	(C_{3}/h^{2})	(C_4/h^2)
										0	(C_0/h^2)	(C_1/h^2)	$(C_2/h^2) +k(x_3)$	(C_{3}/h^{2})	(C_4/h^2)	0
													(0) (0)			
										(,	()	$+k(x_2)$	()	()		
										(C_0/h^2)	(C_1/h^2)	(C_2/h^2)	(C_3/h^2)	(C_4/h^2)	0	0
										(C_0/n^2)	$+k(x_{1})$	(C_2/n^2)	(C_3/n^2)	(C_4/n^2)	0	0
										(C_{2}/h^{2})	(C_1/h^2)	(C_2/h^2)	(C_{2}/h^{2})	(C_1/h_2)	0	0
										$+k(x_0)$	(C_1/n^2)	(C_2/n^2)	(U_3/n^2)	(C_4/n^2)	0	0
										(C_0/h^2)	(C_1/h^2)	(C_2/h^2)	(C_{α}/h^2)	(C_1/h^2)	0	0
									[
	_		_													

(a) Second derivative = blue and green elements (b) Zoom up of the blue enclosed region of the matrix (in k(x) = blue elements Red elements are zero.

FIG. F5. (a) General structure of the H-matrix shown using small sized representation. The numerical derivative are centered on the blue elements and occupy 5 elements on each row, owing to 5-point numerical derivative approximation. Non-derivative term like k(x) are present in the diagonal elements. Other elements are zero (shown in red). (b) A zoom up of the blue enclosed region showing the detailed composition of the respective elements.



FIG. F6. Eigendecomposition of the H-matrix to obtain the eigenvectors, $\psi(x)$ and $\psi^{\dagger}(x)$) in the form of two square matrices, and the eigenvalues as diagonals of a square matrix.

Comparison of the present implementation of the finite difference method with other methods for the solution of 1D Schrödinger equation

To verify our implementation of the above described procedure involving the finite difference approximation for numerical derivative, we compare the results obtained using the same potential on LEVEL16 program by Le Roy[8] which is based on the Cooley method[9]. A comparison of dissociation energies from different vibrational levels is presented in Table T21 showing that a non-systematic difference in dissociation energies (in cm⁻¹) appears on the third digit after decimal for any of the *J*-state. For comparing the accuracy of the wavefunction, a comparison of the matrix elements computed with respective wavefunctions is shown in Table T22 where it is seen that the difference in the numerical value of the matrix element is of the order of 10^{-7} . These comparisons indicate that the present implementation of the procedure based on finite difference approximation is accurate enough for present purpose.

TABLE T21. Comparison of dissociation energies (D_e) for H₂ from different vibrational levels (v=0-4,J=0) obtained from our implementation of procedure described in Section S5 and LEVEL16 program implementing the Cooley method.

v, J	Our program	$\mathbf{LEVEL16}^{\mathrm{a}}$	Δ
0,0	-36118.217	-36118.210	-0.006
$1,\!0$	-31957.282	-31957.281	-0.001
2,0	-28031.632	-28031.627	-0.005
3,0	-24336.385	-24336.379	-0.006
4,0	-20868.501	-20868.493	-0.008
a Ref	. 8		

TABLE T22. Matrix elements (a.u.) for H_2 obtained by wavefunctions from the present implementation of procedure described in Section S5 and LEVEL16 based on the Cooley method.

]	Matrix element	Our program	$\mathbf{LEVEL16}^{\mathrm{a}}$	Δ
H_2	$\langle \psi_{00} ar{lpha} \psi_{00} angle$	5.417943315	5.417943279	0.000000037
	$\langle\psi_{00} \gamma \psi_{00} angle$	2.031207900	2.031207449	0.000000451

^a Ref. 8

S6. Error estimation for matrix elements

In the present work, errors can be introduced from many different sources which have to be identified and the magnitude of each error has to be estimated. The present section is devoted to the details of the identified sources and magnitude of each error.

The potential energies and the corrections were interpolated using cubic spline interpolation procedure while solving the radial nuclear Schrödinger equation. The error introduced by the cubic spline interpolation was estimated by removing each data point one by one and generating new interpolated data which was compared to the original value thus giving information about the maximal oscillation of the cubic spline in the absence of a data point. The maximal shift in the numerical value of the potential and the corrections for the potential was found to be $\sim 10^{-7}$ a.u. A similar analysis on the polarizability data points over distance showed a maximal shift of $\sim 10^{-6}$ a.u.

Any effect of random noise in the potential energy surface was investigated by introducing artificial white noise oscillating within $\pm 1 \times 10^{-6}$ having random statistical distribution. Wavefunctions obtained by such perturbed potentials were used to calculate the matrix elements. This was done for 31 random noise vectors for statistical analysis and the 3σ standard deviation in the values of the matrix elements is shown in Table T23, where it is observed that the effect on the matrix element is below 10^{-5} a.u.

TABLE T23. Effect of random noise (oscillating within $\pm 10^{-6}$ a.u.) in the potential energy on the matrix elements (static)

Matrix element	3 σ
$\langle \psi_{0,0} \gamma \psi_{0,0} angle$	8.7×10^{-6}
$\langle \psi_{0,0} ar{lpha} \psi_{0,0} angle$	7.1×10^{-6}
$\langle \psi_{0,0} \gamma \psi_{0,2} angle$	8.8×10^{-6}
$\langle \psi_{0,0} \bar{\alpha} \psi_{1,0} \rangle$	2.7×10^{-6}

During generation of the H-matrix, the reduced nuclear $mass(\mu)$ of the molecule is required. The masses of proton and deuteron have their respective uncertainties which propagates to the reduced mass and then to the elements of the H-matrix. In order to estimate the maximal error due to uncertainty in nuclear masses, two H-matrices were setup, one with the error added to both the nuclei and second, where the error was subtracted. The resulting wavefunctions were used to calculate the matrix elements, from which the maximal error in respective matrix elements was determined. These are shown in Table T24 where it is seen that the error due to uncertainty of nuclear masses is of the order of 10^{-11} a.u. Among the three isotopologues, due to the smaller nuclear mass of a proton the contribution of error due to nuclear mass is more in H₂, which decreases in HD and is the lowest in D₂.

TABLE T24. Maximal error in the matrix elements (static) due to the uncertainty in nuclear mass

	$\Delta \langle \psi_{0,0} ar{lpha} \psi_{0,0} angle$	$\Delta \langle \psi_{0,0} \gamma \psi_{0,0} angle$
H_2 HD D ₂	$2.5 \times 10^{-11} \\ 1.2 \times 10^{-11} \\ 6.3 \times 10^{-12}$	$\begin{array}{c} 3.6 \times 10^{-11} \\ 1.5 \times 10^{-11} \\ 6.3 \times 10^{-12} \end{array}$

In the presently used technique involving finite differences to solve the 1D Schrödinger equation, the H-matrix is setup using an array of inter-nuclear distance of certain step size. The choice of step size (h) is crucial to obtain resulting wavefunctions of sufficient accuracy. With the step (h) of 0.004 a.u., the truncation error when keeping the Taylor series expansion up to the 4th-order derivative was estimated using Eqn. 8 for the first derivative (see Section S5 B) and a similar equation for the second derivative, giving a net maximal error of the order of 10^{-8} a.u. Effect of the step size and numerical rounding off in computation on the matrix element was estimated by calculating matrix elements of $\bar{\alpha}$ and γ using the wavefunctions obtained from using different step sizes. From this analysis it was found that uncertainty of the order of 10^{-8} a.u. exists due to above mentioned numerical errors and approximations, for any matrix element when h=0.004 a.u. was used.

When computing the wavelength dependent matrix elements of the polarizability invariants, the exact wavelength (say λ_i) at which the matrix element is sought might differ by up to a few nanometers with respect to the wavelength at which the invariant over distance is available (say $\lambda_i \pm q_i$). In the present work, q_i is up to ~5 nm. In such case, there are two ways to compute the matrix element. First, the polarizability

invariant can be interpolated over wavelength to obtain the required invariant as a function of distance for λ_i followed by computation of the matrix element. Secondly, the matrix elements can be computed at $\lambda_i + q_i$ (or $\lambda_i - q_i$) followed by interpolation (of the matrix elements) to obtain an interpolated value at λ_i . Both of these methods were tested to compute the respective matrix element at a given wavelength and the difference was found to be less than 1.0×10^{-7} a.u. revealing the low error in spline interpolation procedure achievable due to the densely spaced polarizability data points over wavelength.

The combined effect of all the errors discussed above, namely error due to spline interpolation, random noise in the potential, uncertainty in nuclear mass, the step size when generating the H-matrix, the uncertainty due to numerical rounding and interpolation of matrix elements over wavelength is no more than $\pm 1 \times 10^{-5}$ a.u. for any matrix element, and we regard this as the maximal numerical error.

S7. Tables of dissociation and transitions energies of H₂, D₂ and HD

Molecule		Г		Expt.			
	Our	Ref. 10	Δ	Others	Δ	Expt.	Δ
H_2	36118.2167	36118.060	0.156	36118.069 ^a	0.147	36118.06962(37) ^b	0.1471
HD	36405.8720	36705.774	0.098	36405.7828 $^{\rm c}$	0.0892	$36405.828(16)^{b}$	0.044
D ₂	36748.4080	36748.355	0.053	36748.363 ^a	0.045	$36748.36286(68)^{\rm d}$	0.0451

TABLE T25. Dissociation energy (cm^{-1}) for H_2 , HD and D_2 .

^a Ref. 11

^b Ref. 12

^c Ref. 13 ^d Ref. 14

			S 0		01						
		Our		$\mathbf{Expt.}$		Our		Expt.			
J_i	Our	Δ^{a}	Δ^{b}	Δ^{c}	Our	Δ^{a}	Δ^{b}	Δ^{d}			
0	354.2035	-0.188	-0.1696	-0.1700							
1	586.7532	-0.279	-0.2788	-0.2789							
2	814.0419	-0.383	-0.3825	-0.3829	3806.7324	-0.043		-0.127			
3	1034.1920	-0.480	-0.4787	-0.4782	3568.2741	0.070		0.035			
4	1245.5336	-0.567	-0.5659	-0.5645	3329.2045	0.180		0.061			
5	1446.6380	-0.644	-0.6429	-0.6408	3091.4729	0.288		0.332			
6	1636.3370	-0.710			2856.8554	0.388					
7	1813.7288				2626.9195						
8	1978.1708				2403.0013						
			Q1				$\mathbf{S1}$				
		Our		$\mathbf{Expt.}$		Our		Expt.			
J_i	Our	Δ^{a}	Δ^{b}	Δ^{e}	Our	Δ^{a}	Δ^{b}	$\Delta^{\mathbf{e}}$			
0	4160.9359	-0.231	-0.2302	-0.2271	4497.4500	-0.391	-0.3884	-0.3891			
1	4155.0273	-0.209	-0.2265	-0.2274	4712.4182	-0.471	-0.4864	-0.4872			
2	4143.2464	-0.203	-0.2189	-0.2196	4916.4310	-0.562	-0.5753	-0.5759			
3	4125.6649	-0.192	-0.2077	-0.2090	5107.7495	-0.641	-0.6534	-0.6545			
4	4102.3891	-0.179	-0.1929	-0.1929	5284.8720	-0.709					
5	4073.5575	-0.162			5446.5641	-0.764					
6	4039.3383	-0.142			5591.8744	-0.805					
7	3999.9261				5720.1347						
8	3955.5374				5830.9481						

TABLE T26. Transition energies (cm^{-1}) for H_2

^a Ref. 10
 ^b Ref. 11
 ^c Ref. 15
 ^d Ref. 16
 ^e Ref. 17

		Theory		
Our	Δ^{a}	Δ^{b}	$\Delta^{\rm c}$	Δ^{d}
3632.0067	-0.147	-0.154	-0.1537	-0.1528
3454.5877	-0.129	-0.129		
3280.6508	-0.109	-0.103		
3109.1838	-0.084	-0.075		
2939.0983	-0.054	-0.046		
2769.1972	-0.023	-0.017		

TABLE T27. $\Delta G(v+1/2)$ (cm⁻¹) for HD

^a Ref. 10 ^b Ref. 18 ^c Ref. 13 ^d Ref. 19

Transition	Theo	Expt.	
	Our	Δ^{a}	Δ^{b}
P1(3)	3355.3165	-0.052	-0.044
P1(2)	3450.3752	-0.085	-0.088
P1(1)	3542.8109	-0.118	-0.121
R1(0)	3717.3482	-0.181	-0.184
R1(1)	3798.2393	-0.210	-0.216
R1(2)	3874.1158	-0.236	-0.241
R1(3)	3944.4594	-0.260	-0.261
R1(4)	4008.8087	-0.279	-0.279
^a Ref 10			

TABLE T28. $P_v(J)$ and $R_v(J)$ line positions (cm⁻¹) for HD

^b Ref. 20

TABLE T29. Transition energies (cm^{-1}) for D_2

			S 0				01	
		Our		Expt.		Our		Expt.
J_i	Our	Δ^{a}	Δ^{b}	Δ^{c}	Our	Δ^{a}	Δ^{b}	Δ^{d}
0	179.0239	-0.045	-0.043	-0.044				
1	297.4623	-0.072	-0.071	-0.071				
2	414.5495	-0.099	-0.099	-0.099	2814.507	-0.032	-0.043	-0.039
3	529.7747	-0.126	-0.125	-0.125	2693.960	-0.003	-0.013	-0.012
4	642.6558	-0.151	-0.150	-0.150	2572.660	0.025	0.015	0.017
5	752.7452	-0.176	-0.174	-0.178	2451.132	0.053		
6	859.6354	-0.198	-0.197	-0.210	2329.879	0.081		
$\overline{7}$	962.9626	-0.217			2209.372	0.109		
8	1062.4090	-0.236			2090.051	0.893		
			Q 1				S 1	
		Our		$\mathbf{Expt.}$		Our		$\mathbf{Expt.}$
J_i	Our	Δ^{a}	Δ^{b}	Δ^{d}	Our	Δ^{a}	Δ^{b}	Δ^{d}
0	2993.5309	-0.077	-0.1017	-0.0827	3166.2333	-0.119	-0.1272	-0.1263
1	2991.4216	-0.075	-0.0854	-0.0862	3278.3696	-0.143	-0.1535	-0.1526
2	2987.2093	-0.074	-0.0841	-0.0809	3387.0842	-0.169	-0.1784	-0.1764
3	2980.9073	-0.072	-0.0821	-0.0778	3491.8920	-0.192	-0.2017	-0.1993
4	2972.5350	-0.070	-0.0791		3592.3424	-0.215		
5	2962.1173	-0.067			3688.0251	-0.234		
6	2949.6866	-0.063			3778.5753	-0.252		
$\overline{7}$	2935.2800	-0.058			3863.6767	-0.266		
8	2918.9400	-0.054			3943.0637	-0.279		

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^a Ref. 10 ^b Ref. 11 ^c Ref. 21 ^d Ref. 22

Molecule			$\langle \psi_{v,J} \gamma \psi_v$,', _J '				$\langle \psi_{v,J} ar{lpha} \psi_{v,J} $	$_{v',J'}\rangle$	
	$\ket{v,J}$	v',J' angle	Our	Ref. 1	Δ	$\ket{v,J}$	v',J' angle	Our	Ref. 1	Δ
H_2	$ 0,0\rangle$	$ 0,2\rangle$	2.1524	2.1514	0.0010	$ 0,0\rangle$	$ 1,0\rangle$	0.7879	0.7883	-0.0004
	$ 0,1\rangle$	$ 0,3\rangle$	2.1686	2.1677	0.0009	$ 0,1\rangle$	$ 1,1\rangle$	0.7891	0.7895	-0.0004
	$ 0,2\rangle$	$ 0,4\rangle$	2.1929	2.1920	0.0009	$ 0,2\rangle$	$ 1,2\rangle$	0.7915	0.7919	-0.0004
	0,3 angle	$ 0,5\rangle$	2.2255	2.2246	0.0009	0,3 angle	$ 1,3\rangle$	0.7951	0.7955	-0.0004
	$ 1,0\rangle$	$ 1,2\rangle$	2.6651	2.6641	0.0010					
	$ 1,1\rangle$	$ 1,3\rangle$	2.6824	2.6815	0.0009					
	$ 1,2\rangle$	$ 1,4\rangle$	2.7085	2.7075	0.0010					
	1,3 angle	$ 1,5\rangle$	2.7432	2.7423	0.0009					
HD	$ 0,0\rangle$	$ 0,2\rangle$	2.1161	2.1151	0.0010	$ 0,0\rangle$	$ 1,0\rangle$	0.7299	0.7303	-0.0004
	$ 0,1\rangle$	$ 0,3\rangle$	2.1282	2.1272	0.0010	$ 0,1\rangle$	$ 1,1\rangle$	0.7307	0.7311	-0.0004
	$ 0,2\rangle$	$ 0,4\rangle$	2.1464	2.1454	0.0010	$ 0,2\rangle$	$ 1,2\rangle$	0.7324	0.7328	-0.0004
	0,3 angle	$ 0,5\rangle$	2.1706	2.1697	0.0009	0,3 angle	1,3 angle	0.7349	0.7353	-0.0004
	$ 1,0\rangle$	$ 1,2\rangle$	2.5535	2.5525	0.0010					
	$ 1,1\rangle$	$ 1,3\rangle$	2.5664	2.5654	0.0010					
	$ 1,2\rangle$	$ 1,4\rangle$	2.5857	2.5847	0.0010					
	$ 1,3\rangle$	$ 1,5\rangle$	2.6115	2.6105	0.0010					
D_2	$ 0,0\rangle$	$ 0,2\rangle$	2.0742	2.0732	0.0010	$ 0,0\rangle$	$ 1,0\rangle$	0.6559	0.6563	-0.0004
_	$ 0,1\rangle$	$ 0,3\rangle$	2.0822	2.0812	0.0010	$ 0,1\rangle$	$ 1,1\rangle$	0.6564	0.6568	-0.0004
	$ 0,2\rangle$	$ 0,4\rangle$	2.0942	2.0933	0.0009	$ 0,2\rangle$	$ 1,2\rangle$	0.6575	0.6578	-0.0003
	0,3 angle	0,5 angle	2.1103	2.1094	0.0009	0,3 angle	1,3 angle	0.6590	0.6593	-0.0003
	$ 1,0\rangle$	$ 1,2\rangle$	2.4250	2.4239	0.0011					
	$ 1,1\rangle$	$ 1,3\rangle$	2.4334	2.4324	0.0010					
	$ 1,2\rangle$	$ 1,4\rangle$	2.4461	2.4451	0.0010					
	$ 1,3\rangle$	$ 1,5\rangle$	2.4631	2.4620	0.0011					

TABLE T30. Comparison of present rotationally averaged mean polarizability and anisotropy with the theoretical results of Schwartz and Le Roy (Ref. 1) at 488 nm.

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